

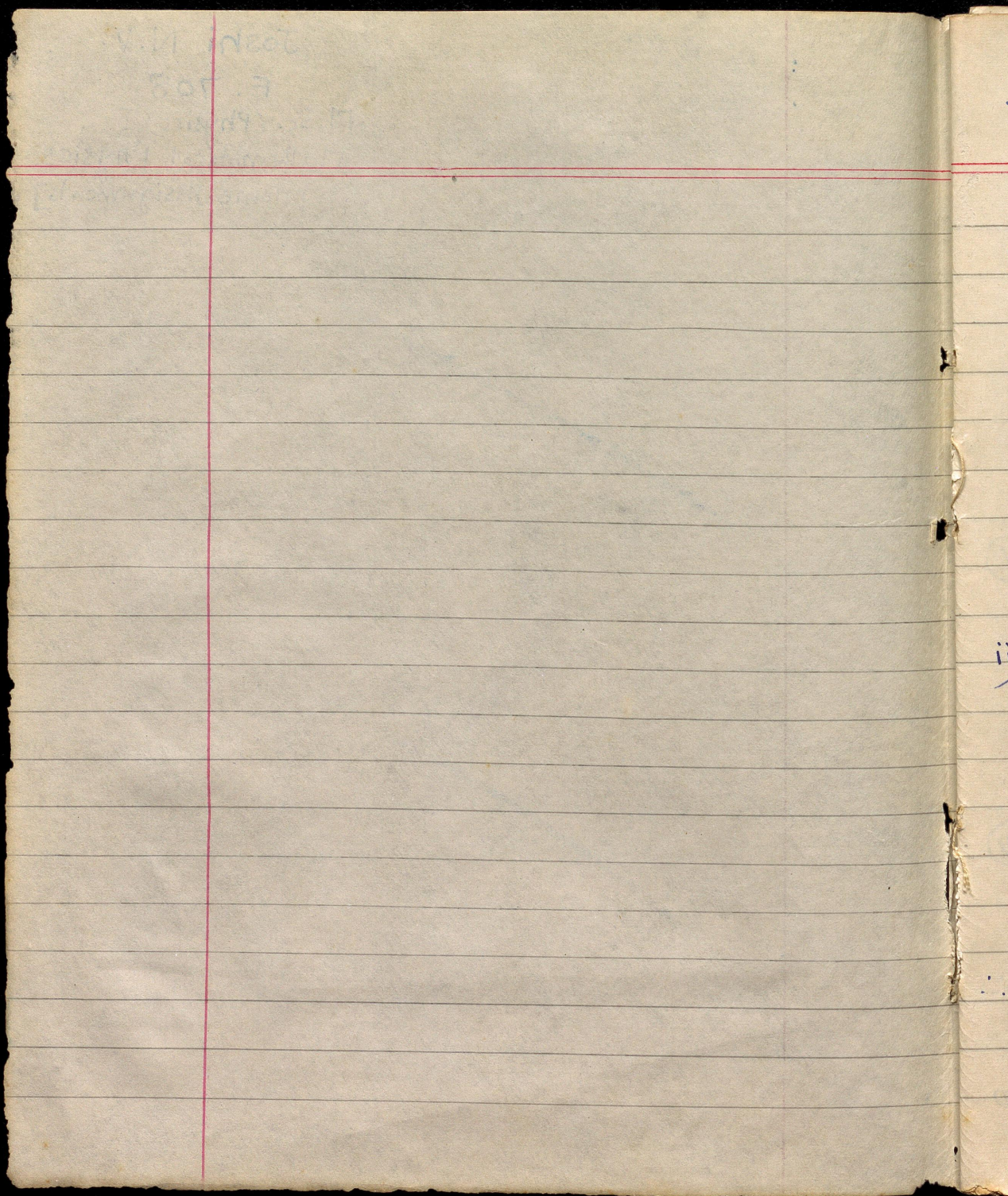
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F. 708

M.Sc. (Physics) I

Mathematical Physics

[Home Assignments]



i) If \vec{a} , \vec{b} & \vec{c} are coplanar vectors, and $\vec{b} \times \vec{c}$ then it is possible to write

$$\vec{a} = \alpha \vec{b} + \beta \vec{c}$$

From the starting pt. of \vec{a} , say O, draw $\vec{ON} \parallel \vec{b}$ & $\vec{OM} \parallel \vec{c}$, such that ONAM is a parallelogram.

Now $\vec{ON} \parallel \vec{b} \Rightarrow \exists$ scalar α such that $\vec{ON} = \alpha \vec{b}$

$\vec{OM} \parallel \vec{c} \Rightarrow \exists$ scalar β such that $\vec{OM} = \beta \vec{c}$

Now by law of parallelogram of forces,

$$\vec{a} = \vec{OA} = \vec{OM} + \vec{ON} \quad \text{but } \vec{ON} = \alpha \vec{b}, \vec{OM} = \beta \vec{c}$$

$$\therefore \vec{a} = \alpha \vec{b} + \beta \vec{c} \quad \text{q.e.d.}$$

ii) If \vec{a} , \vec{b} , \vec{c} are coplanar,

$$\begin{vmatrix} c_1 & c_2 & c_3 \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix} = 0.$$

\vec{a} , \vec{b} , \vec{c} coplanar $\Rightarrow \exists$ scalars α, β such that

$$\vec{a} = \alpha \vec{b} + \beta \vec{c}$$

$$\Rightarrow a_1 = \alpha b_1 + \beta c_1, a_2 = \alpha b_2 + \beta c_2, a_3 = \alpha b_3 + \beta c_3$$

$$\begin{vmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix} = \begin{vmatrix} \alpha b_1 & \alpha b_2 & \alpha b_3 \\ \beta c_1 & \beta c_2 & \beta c_3 \\ b_1 & b_2 & b_3 \end{vmatrix} = \alpha \begin{vmatrix} c_1 & c_2 & c_3 \\ b_1 & b_2 & b_3 \end{vmatrix} + \beta \begin{vmatrix} c_1 & c_2 & c_3 \\ b_1 & b_2 & b_3 \end{vmatrix}$$

$= 0$ since two rows are identical in both the determinants.

(iii) Show that $\bar{a} \cdot \bar{b}$ is invariant under transformation of co-ordinates
i.e. $\bar{a} \cdot \bar{b} = \underline{a} \cdot \underline{b}$

$$\begin{aligned}
 \text{We have } \bar{a} \cdot \bar{b} &= \sum_p a_p b_p \\
 &= \sum_{i,j,p} a_i l_{ip} b_j l_{jp} \\
 &= \sum_{i,j} a_i b_j \left(\sum_p l_{ip} l_{jp} \right) \\
 &= \sum_{i,j} a_i b_j \delta_{ij} \\
 &= \sum_i a_i b_i = \underline{a} \cdot \underline{b} \quad \text{q.e.d.}
 \end{aligned}$$

(iv) $\bar{a} \times (\bar{b} \times \bar{c}) = \bar{b} (\bar{a} \cdot \bar{c}) - \bar{c} (\bar{a} \cdot \bar{b})$

$$\begin{aligned}
 \text{LHS} &= \bar{a} \times (\bar{b} \times \bar{c}) \\
 &= \sum_l a_l e_{(l)} \times \sum_{ijk} \epsilon_{ijk} b_i c_j e_{(k)} \\
 &= \sum_{ijk\ell} \epsilon_{ijk} a_\ell b_i c_j [e_{(l)} \times e_{(k)}] \\
 &= \sum_{ijklmnp} \epsilon_{ijk} \epsilon_{mnp} a_\ell b_i c_j e_{(l)m} e_{(k)n} \hat{e}_{(p)} \\
 &= \sum_{ijklmnp} \epsilon_{ijk} \epsilon_{mnp} a_\ell b_i c_j \delta_{\ell m} \delta_{kn} \hat{e}_{(p)}
 \end{aligned}$$

$$= \sum_{ijkp} \epsilon_{ijk} \epsilon_{knp} a_i b_j c_j e_{(p)}$$

$$= \sum_{ijkp} (d_{ip} d_{je} - d_{ie} d_{jp}) a_i b_j c_j e_{(p)}$$

$$= \sum_{ij} a_j b_i c_j e_{(i)} - \sum_{ij} a_i b_i c_j e_{(j)}$$

$$= \left[\sum_i b_i e_{(i)} \right] \sum_j a_j c_j - \left[\sum_j c_j e_{(j)} \right] \sum_i a_i b_i$$

$$= \bar{b} (\bar{a} \cdot \bar{c}) - \bar{c} (\bar{a} \cdot \bar{b}) = \text{RHS} \quad \text{q.e.d.}$$

$$\textcircled{v} \quad \bar{a} \times (\bar{b} \times \bar{c}) + \bar{b} \times (\bar{c} \times \bar{a}) + \bar{c} \times (\bar{a} \times \bar{b}) = 0$$

$$\begin{aligned} \text{LHS} &= \bar{b} (\bar{a} \cdot \bar{c}) - \bar{c} (\bar{a} \cdot \bar{b}) \\ &+ \bar{c} (\bar{b} \cdot \bar{a}) - \bar{a} (\bar{b} \cdot \bar{c}) \\ &+ \bar{a} (\bar{b} \cdot \bar{c}) - \bar{b} (\bar{c} \cdot \bar{a}) \\ &= 0 = \text{R.H.S.} \quad \text{q.e.d.} \end{aligned}$$

$$\textcircled{vi} \quad (\bar{a} \cdot \hat{e}) \hat{e} + \hat{e} \times (\bar{a} \times \hat{e}) = \bar{a}$$

Now, we have

$$\hat{e} \times (\bar{a} \times \hat{e}) = \bar{a} (\hat{e} \cdot \hat{e}) - \hat{e} (\bar{a} \cdot \hat{e})$$

$$\therefore \text{LHS} = (\bar{a} \cdot \hat{e}) \hat{e} + \hat{e} (\bar{a} \times \hat{e})$$

$$= (\bar{a} \cdot \hat{e}) \hat{e} + \bar{a} (\hat{e} \cdot \hat{e}) - (\bar{a} \cdot \hat{e}) \hat{e}$$

$$= \bar{a} (\hat{e} \cdot \hat{e}) = \bar{a} = \text{RHS}$$

since \hat{e} is a unit vector $\Rightarrow \hat{e} \cdot \hat{e} = 1$.

$$\textcircled{\text{vii}} \quad (\bar{a} \times \bar{b}) \cdot (\bar{c} \times \bar{d}) = \begin{vmatrix} \bar{a} \cdot \bar{c} & \bar{a} \cdot \bar{d} \\ \bar{b} \cdot \bar{c} & \bar{b} \cdot \bar{d} \end{vmatrix}$$

$$\text{L.H.S.} = (\bar{a} \times \bar{b}) \cdot \bar{m} \quad \text{where } \bar{m} = \bar{c} \times \bar{d}$$

$$= \bar{a} \cdot (\bar{b} \times \bar{m})$$

$$= \bar{a} \cdot [\bar{b} \times (\bar{c} \times \bar{d})]$$

$$= \bar{a} \cdot [\bar{c}(\bar{b} \cdot \bar{d}) - \bar{d}(\bar{b} \cdot \bar{c})]$$

$$= (\bar{a} \cdot \bar{c})(\bar{b} \cdot \bar{d}) - (\bar{b} \cdot \bar{c})(\bar{a} \cdot \bar{d})$$

$$= \begin{vmatrix} \bar{a} \cdot \bar{c} & \bar{a} \cdot \bar{d} \\ \bar{b} \cdot \bar{c} & \bar{b} \cdot \bar{d} \end{vmatrix} = \text{R.H.S.} =$$

$$\textcircled{\text{viii}} \quad \{ \bar{a} \times \bar{b} \} \times \{ \bar{c} \times \bar{d} \} = \{ \bar{a} \cdot (\bar{b} \times \bar{d}) \} \bar{c} - \{ \bar{a} \cdot (\bar{b} \times \bar{c}) \} \bar{d}$$

$$\text{L.H.S.} = \bar{a} \times \{ \bar{b} \times (\bar{c} \times \bar{d}) \}$$

$$= \bar{b} \{ \bar{a} \cdot (\bar{c} \times \bar{d}) \} - (\bar{c} \times \bar{d}) \{ \bar{a} \cdot \bar{b} \}$$

$$\text{L.H.S.} = \{ \bar{a} \times \bar{b} \} \times \{ \bar{c} \times \bar{d} \}$$

$$= \bar{c} \{ (\bar{a} \times \bar{b}) \cdot \bar{d} \} - \bar{d} \{ (\bar{a} \times \bar{b}) \cdot \bar{c} \}$$

$$= \{ \bar{a} \cdot \bar{b} \times \bar{d} \} \bar{c} - \{ \bar{a} \cdot \bar{b} \times \bar{c} \} \bar{d}$$

$$= \text{R.H.S.}$$

(ix) $L = \begin{vmatrix} l_{11} & l_{12} & l_{13} \\ l_{21} & l_{22} & l_{23} \\ l_{31} & l_{32} & l_{33} \end{vmatrix} = 1$ using orthonormality of vectors.

$$L = l_{11}(l_{22}l_{33} - l_{23}l_{32}) + l_{12}(l_{23}l_{31} - l_{21}l_{33}) + l_{13}(l_{21}l_{32} - l_{22}l_{31}) \quad \text{--- (d)}$$

Now $e_{(1)1} = [\hat{e}_{(2)} \times \hat{e}_{(3)}] \cdot \hat{e}_{(1)}$

$$= \left\{ \sum_{ijk} \epsilon_{ijk} e_{(2)i} e_{(3)j} e_k \right\} \cdot \hat{e}_{(1)} \quad \text{--- (a)}$$

$$= e_{(2)2} \cdot e_{(3)3} - e_{(2)3} e_{(3)2}$$

Hence $l_{11} = l_{22}l_{33} - l_{23}l_{32}$

Similarly, we have

$$e_{1(2)} = [\hat{e}_{(2)} \times \hat{e}_{(3)}] \cdot \hat{e}_{(2)}$$

$$= \left\{ \sum_{ijk} \epsilon_{ijk} e_{(2)i} e_{(3)j} e_k \right\} \cdot \hat{e}_{(2)} \quad \text{--- (b)}$$

$$= e_{(2)1} e_{(3)3} - e_{(2)3} e_{(3)1}$$

$$\therefore l_{12} = l_{23}l_{31} - l_{21}l_{33} \quad \text{--- (b)}$$

$$\text{simly } l_{13} = l_{21}l_{32} - l_{22}l_{31} \quad \text{--- (c)}$$

substituting (a), (b), (c) in (d)

$$L = l_{11}^2 + l_{12}^2 + l_{13}^2 = 1 = \text{R.H.S.}$$

(x) If (m_1, m_2, m_3) and (μ_1, μ_2, μ_3) are such that $\sum_i a_i m_i = \sum_p a_p \mu_p$ then m_1, m_2, m_3 are components of a vector.

Now,

$$\sum_p a_p \mu_p = \sum_p \left[\sum_i a_i \mu_{ip} \right] \mu_p$$

$$= \sum_{ip} a_i \mu_{ip} \mu_p$$

Now $\sum_p \mu_{ip} \mu_p = m_i$

$$\therefore \sum_{ip} a_i \mu_{ip} \mu_p = \sum_i a_i m_i$$

$$\therefore \sum_i \left(\sum_p \mu_{ip} \mu_p - m_i \right) a_i = 0.$$

$$a_i \neq 0 \Rightarrow m_i = \sum_p \mu_{ip} \mu_p$$

hence (m_1, m_2, m_3) is a vector
are components of a vector.

(xi) (a) $\nabla \frac{1}{r}$

$$= \sum_i e_{(i)} \frac{\partial}{\partial x_i} \left(\frac{1}{r} \right)$$

$$= -\frac{1}{r^2} \sum_i e_{(i)} \frac{\partial}{\partial x_i} \left(\sqrt{x_1^2 + x_2^2 + x_3^2} \right)$$

$$\begin{aligned} \therefore \nabla \frac{1}{r} &= \frac{1}{r^2} \sum e_{(i)} \frac{x_i}{r} \\ &= \frac{\bar{r}}{r^3} \end{aligned}$$

$$\begin{aligned} b) \nabla r^n &= \sum_i \frac{\partial}{\partial x_i} r^n e_{(i)} \\ &= n r^{n-1} \sum \frac{\partial (r)}{\partial x_i} e_{(i)} \\ &= n r^{n-2} \bar{r} \end{aligned}$$

c) $\nabla(\bar{e} \cdot \bar{r})$ where \bar{e} is a constant vector

$$\nabla(\bar{e} \cdot \bar{r}) = \nabla \left(\sum_i e_i x_i \right)$$

$$= \sum_{ij} \hat{e}_{(j)} \frac{\partial}{\partial x_j} (e_i x_i)$$

$$= \sum_{ij} \hat{e}_{(j)} e_i \frac{\partial x_i}{\partial x_j} \quad \text{since } \frac{\partial e_i}{\partial x_j} = 0$$

$$= \sum_{ij} \hat{e}_{(j)} e_i \delta_{ij}$$

$$= \sum_i \hat{e}_{(i)} e_i$$

$$= \bar{e}$$

(xii) Show that $\nabla \cdot \bar{a}$ is invariant under the rotation of axes.

$$\begin{aligned}\nabla \cdot \bar{a} &= \sum_p \frac{\partial}{\partial x_p} a_p \\ &= \sum_{p, i, j} \frac{\partial a_j}{\partial x_i} \delta_{ip} \delta_{jp} \\ &= \sum_{p, i, j} \frac{\partial a_j}{\partial x_i} \delta_{ij} \\ &= \sum_i \frac{\partial a_i}{\partial x_i} = \nabla \cdot \bar{a} \quad \text{q.e.d.}\end{aligned}$$

(xiii) For two dimensional motion.

$$\bar{\omega} = \frac{1}{2} \left(\frac{\partial v_2}{\partial x_1} - \frac{\partial v_1}{\partial x_2} \right)$$

$$\nabla \times \bar{v} = \sum_{i, j, k} \epsilon_{ijk} \frac{\partial v_j}{\partial x_i} e_k$$

But for two dimensional motion, only one component of $\bar{\omega}$ exists.

$$\begin{aligned}\nabla \times \bar{v} &= \sum_{i, j} \epsilon_{ij3} \frac{\partial v_j}{\partial x_i} \\ &= \frac{\partial v_2}{\partial x_1} - \frac{\partial v_1}{\partial x_2}\end{aligned}$$

$$\text{but } |\nabla \times \bar{v}| = |\nabla \times (\bar{\omega} \times \bar{r})| = 2\omega$$

$$\therefore 2\omega = \frac{\partial v_2}{\partial x_1} - \frac{\partial v_1}{\partial x_2}$$

$$\therefore \omega = \frac{1}{2} \left[\frac{\partial v_2}{\partial x_1} - \frac{\partial v_1}{\partial x_2} \right] \quad \text{q.e.d.}$$

(xiv) Show that

$$\nabla \times (\phi \bar{A}) = \nabla \phi \times \bar{A} + \phi (\nabla \times \bar{A})$$

$$\text{L.H.S.} = \sum_{ijk} \epsilon_{ijk} \frac{\partial}{\partial x_i} (\phi A_j) \hat{e}_k$$

$$= \sum_{ijk} \left(\frac{\partial \phi}{\partial x_i} A_j + \phi \frac{\partial A_j}{\partial x_i} \right) \epsilon_{ijk} \hat{e}_k$$

$$= \sum_{ijk} \epsilon_{ijk} \frac{\partial \phi}{\partial x_i} A_j \hat{e}_k + \phi \sum_{ijk} \epsilon_{ijk} \frac{\partial A_j}{\partial x_i} \hat{e}_k$$

$$= \nabla \phi \times \bar{A} + \phi (\nabla \times \bar{A}) \quad \text{q.e.d.}$$

(xv)

$$\nabla \cdot (f \bar{v}) = \nabla f \cdot \bar{v} + f (\nabla \cdot \bar{v})$$

$$\text{L.H.S.} = \sum_i \frac{\partial}{\partial x_i} f v_i$$

$$= \sum_i \left[\frac{\partial f}{\partial x_i} v_i + f \frac{\partial v_i}{\partial x_i} \right]$$

$$= \sum_i \frac{\partial f}{\partial x_i} v_i + f \sum_i \frac{\partial v_i}{\partial x_i}$$

$$= \nabla f \cdot \bar{v} + f (\nabla \cdot \bar{v})$$

Thus

$$\nabla \cdot (f \bar{v}) = \nabla f \cdot \bar{v} + f (\nabla \cdot \bar{v}) \quad \text{q.e.d.}$$

(xvi) $\bar{A} = \bar{\alpha} \times \bar{\beta}$ $\bar{\alpha}$ is a constant vector

Find $\nabla \cdot \bar{A}$

$$\nabla \cdot \bar{A} = \sum_l \hat{e}_l \frac{\partial}{\partial x_l} \bar{A}_l = \sum_{ijk} \epsilon_{ijk} \alpha_i \beta_j \hat{e}_k$$

$$= \sum_{ijk} \frac{\partial}{\partial x_l} (\alpha_i \beta_j) \delta_{lk} \epsilon_{ijk}$$

$$= \sum_{ijk} \epsilon_{ijk} \alpha_i \frac{\partial \beta_j}{\partial x_k}$$

$$= \sum_{ijk} \epsilon_{ijk} \alpha_i \frac{\partial \beta_j}{\partial x_k} \hat{e}_{(i)} \cdot \hat{e}_{(i)}$$

$$= \sum_i \alpha_i \hat{e}_{(i)} \cdot \sum_{ijk} \epsilon_{ijk} \frac{\partial \beta_j}{\partial x_k} \hat{e}_{(i)}$$

$$= -\bar{\alpha} \cdot \sum_{ijk} \epsilon_{jki} \frac{\partial \beta_j}{\partial x_k} \hat{e}_{(i)}$$

$$= -\bar{\alpha} \cdot (\nabla \times \bar{\beta})$$

(xvii) $\bar{A} = \psi \nabla \phi - \phi \nabla \psi$

To show that

$$\iiint_V [\psi \nabla^2 \phi - \phi \nabla^2 \psi] dv$$

$$= \oiint (\psi \frac{\partial \phi}{\partial n} - \phi \frac{\partial \psi}{\partial n}) \cdot d\vec{s}$$

By Green's thm -

$$\iiint_V \nabla \cdot \bar{A} \, dV = \iint_S \bar{A} \cdot d\bar{s}$$

$$\therefore \iiint_V \nabla \cdot (\psi \nabla \phi - \phi \nabla \psi) \, dV = \iint_S (\psi \nabla \phi - \phi \nabla \psi) \cdot d\bar{s}$$

$$\text{LHS} = \iiint_V (\psi \nabla^2 \phi + \nabla \psi \cdot \nabla \phi - \nabla \phi \cdot \nabla \psi - \phi \nabla^2 \psi) \, dV$$

$$= \iiint_V [\psi \nabla^2 \phi - \phi \nabla^2 \psi] \, dV$$

$$= \iint_S [\psi \nabla \phi - \phi \nabla \psi] \cdot d\bar{s} = \text{RHS} \quad \text{q.e.d.}$$

xviii

$$\text{Show that } V \bar{x} = \frac{1}{3} \iint_S \bar{x} \cdot d\bar{s}$$

$$= \iiint_V \nabla \cdot \bar{x} \, dV \quad \text{by Green's thm.}$$

$$= \iiint_V 3 \, dV$$

$$= 3 \iiint_V dV = 3V$$

$$\therefore V = \frac{1}{3} \iint_S \bar{x} \cdot d\bar{s} \quad \text{q.e.d.}$$

(xix) Show that

$$\oiint_S \{ \bar{A} (\bar{A} \cdot \bar{n}) - \frac{1}{2} A^2 \bar{n} \} \cdot d\bar{s}$$

$$= \iiint_V \{ \bar{A} (\nabla \cdot \bar{A}) - \bar{A} \times \nabla \times \bar{A} \} dV$$

Now

$$\oiint_S \bar{A} (\bar{A} \cdot \bar{n}) \cdot d\bar{s}$$

$$= \oiint_S \bar{A} \cdot \bar{A} \cdot d\bar{s} \quad \oiint_S A^2 d\bar{s}$$

$$= \iiint_V \nabla \cdot A^2 dV$$

$$= \iiint_V 2 \nabla \cdot \bar{A} dV$$

$$\iiint_S \frac{1}{2} A^2 \bar{n} \cdot d\bar{s} = \iiint_S \frac{A^2}{2} d\bar{s}$$

$$= \iiint_V \nabla \cdot \left(\frac{A^2}{2} \right) dV$$

=

(xix) $J = \text{heat flowing/unit area/unit time} = -k \nabla T$

To prove that eqn. of heat conduction

$$k \nabla^2 T = c e \frac{\partial T}{\partial t} \quad \text{where } c = \text{sp. heat} \\ e = \text{density.}$$

Heat inflow in volume V enclosed by $d\vec{s}$

$$= \oint_S (-k \nabla T) \cdot d\vec{s}$$

$$= \iiint_V \nabla \cdot (-k \nabla T) dV$$

$$= \iiint_V -k \nabla^2 T dV$$

Now, if e is the density & c is the sp. heat
heat absorbed by unit volume/unit time

$$= \iiint_V e c dV \cdot \frac{\partial T}{\partial t} \quad e c dV \frac{\partial T}{\partial t}$$

\therefore Total heat absorbed / unit time

$$= \iiint_V e c \frac{\partial T}{\partial t} dV$$

$$\therefore k \nabla^2 T = c e \frac{\partial T}{\partial t}$$

(22) If $\Phi = \bar{\alpha} \phi$ where $\bar{\alpha}$ is a constant

Show that $\iint_S (\hat{n} \times \nabla \phi) d\bar{s} = \oint_C \phi d\bar{l}$

$$\nabla \times \bar{\alpha} \phi = \bar{\alpha} \times \nabla \phi$$

$$\therefore \iint_S (\nabla \times \bar{\alpha} \phi) d\bar{s} = \iint_S (\bar{\alpha} \times \nabla \phi) \cdot \bar{n} ds$$

$$= \iint_S \bar{\alpha} \cdot (\nabla \phi \times \bar{n}) ds$$

$$= \bar{\alpha} \iint_S (\nabla \phi \times \bar{n}) ds$$

Applying Stokes's thm.

$$\iint_S (\nabla \times \bar{\alpha} \phi) \cdot d\bar{s} = \oint_C (\bar{\alpha} \phi) \cdot d\bar{l}$$

$$= \bar{\alpha} \oint_C \phi d\bar{l}$$

$$\therefore \bar{\alpha} \iint_S (\nabla \phi \times \hat{n}) ds = \bar{\alpha} \oint_C \phi d\bar{l}$$

$$\therefore \iint_S (\nabla \phi \times \bar{n}) ds = \oint_C \phi d\bar{l}$$

q.e.d.

(2xi)

$$\vec{\alpha} \times \vec{\beta} = \vec{A}$$

To prove that $\iint_S (d\vec{s} \times \nabla) \times \vec{\beta} = \oint_C (d\vec{l} \times \vec{\beta})$

Now

$$\iint_S \nabla \times \vec{A} \cdot d\vec{s} = \oint \vec{A} \cdot d\vec{l}$$

$$\therefore \iint_S \nabla \times (\vec{\alpha} \times \vec{\beta}) \cdot d\vec{s} = \oint_C (\vec{\alpha} \times \vec{\beta}) \cdot d\vec{l}$$

$$\text{Now } \nabla \times (\vec{\alpha} \times \vec{\beta}) = \vec{\alpha} \times (\nabla \times \vec{\beta})$$

$$\therefore \iint_S \{ \vec{\alpha} \times (\nabla \times \vec{\beta}) \} \cdot d\vec{s} = \oint (\vec{\alpha} \times \vec{\beta}) \cdot d\vec{l}$$

$$\therefore \iint_S \vec{\alpha} \cdot [(\nabla \times \vec{\beta}) \times d\vec{s}] = \oint \vec{\alpha} \cdot (\vec{\beta} \times d\vec{l})$$

$$\therefore \iint_S (\nabla \times \vec{\beta}) \times d\vec{s} = \oint (\vec{\beta} \times d\vec{l}) \quad \text{q.e.d.}$$

~~V. Good~~
Chalal
14/9/12

Prove that the Jacobian of transformation for a volume element

(24)

$$J \left(\begin{matrix} x_1 & x_2 & x_3 \\ q_1 & q_2 & q_3 \end{matrix} \right) = \sum_{ijk} \epsilon_{ijk} \frac{\partial x_i}{\partial q_1} \frac{\partial x_j}{\partial q_2} \frac{\partial x_k}{\partial q_3}$$

We have, the infinitesimal volume element

$$dV = d\bar{x}_1 \cdot (d\bar{x}_2 \times d\bar{x}_3)$$

$$\text{Using } d\bar{x}_i = \frac{\partial x_i}{\partial q_1} dq_1 + \frac{\partial x_i}{\partial q_2} dq_2 + \frac{\partial x_i}{\partial q_3} dq_3$$

$$\text{We get } dV = d\bar{x}_1 \cdot (d\bar{x}_2 \times d\bar{x}_3)$$

$$= \begin{vmatrix} \frac{\partial x_1}{\partial q_1} dq_1 & \frac{\partial x_1}{\partial q_2} dq_2 & \frac{\partial x_1}{\partial q_3} dq_3 \\ \frac{\partial x_2}{\partial q_1} dq_1 & \frac{\partial x_2}{\partial q_2} dq_2 & \frac{\partial x_2}{\partial q_3} dq_3 \\ \frac{\partial x_3}{\partial q_1} dq_1 & \frac{\partial x_3}{\partial q_2} dq_2 & \frac{\partial x_3}{\partial q_3} dq_3 \end{vmatrix}$$

Since all the elements in column 1 are multiplied by dq_1 , we can take it outside the determinant.

Same holds for dq_2 & dq_3

$$dV = \begin{vmatrix} \frac{\partial x_1}{\partial q_1} & \frac{\partial x_1}{\partial q_2} & \frac{\partial x_1}{\partial q_3} \\ \frac{\partial x_2}{\partial q_1} & \frac{\partial x_2}{\partial q_2} & \frac{\partial x_2}{\partial q_3} \\ \frac{\partial x_3}{\partial q_1} & \frac{\partial x_3}{\partial q_2} & \frac{\partial x_3}{\partial q_3} \end{vmatrix} dq_1 dq_2 dq_3$$

$$\therefore [dx_1 dx_2 dx_3] = J \left(\begin{matrix} x_1 & x_2 & x_3 \\ q_1 & q_2 & q_3 \end{matrix} \right) [dq_1 dq_2 dq_3] \text{ q.e.d.}$$

(25) Determine the volume element in cylindrical co-ordinates

$$x_1 = r \cos \theta \quad x_2 = r \sin \theta \quad x_3 = x_3$$

we have

$$dx_1 dx_2 dx_3 = h_1 h_2 h_3 dq_1 dq_2 dq_3$$

$$h_1^2 = \sum_i \left(\frac{\partial x_i}{\partial q_1} \right)^2 = \sum_{i=1}^3 \left(\frac{\partial x_i}{\partial r} \right)^2 = \cos^2 \theta + \sin^2 \theta + 0 = 1$$

$$\therefore h_1 = 1$$

$$h_2^2 = \sum_{i=1}^3 \left(\frac{\partial x_i}{\partial \theta} \right)^2 = r^2 \sin^2 \theta + r^2 \cos^2 \theta + 0 = r^2 \Rightarrow h_2 = r$$

$$h_3^2 = \sum_{i=1}^3 \left(\frac{\partial x_i}{\partial x_3} \right)^2 = 0 + 0 + 1 = 1 \Rightarrow h_3 = 1$$

$$\therefore dV = 1 \times r \times 1 dq_1 dq_2 dq_3 \\ = r dr d\theta dx_3$$

(26) Determine the volume element in spherical polar co-ords

$$x_1 = r \sin \theta \cos \phi \quad x_2 = r \sin \theta \sin \phi \quad x_3 = r \cos \theta$$

we have, as explained in (25)

$$h_1^2 = \sin^2 \theta \cos^2 \phi + \sin^2 \theta \sin^2 \phi + \cos^2 \theta = 1 \Rightarrow h_1 = 1$$

$$h_2^2 = r^2 \cos^2 \phi \cos^2 \theta + r^2 \sin^2 \phi \cos^2 \theta + r^2 \sin^2 \theta = r^2 \Rightarrow h_2 = r$$

$$h_3^2 = r^2 \sin^2 \theta \sin^2 \phi + r^2 \sin^2 \theta \cos^2 \phi + 0 = r^2 \sin^2 \theta \Rightarrow h_3 = r \sin \theta$$

Now

$$dV = h_1 h_2 h_3 dq_1 dq_2 dq_3$$

$$\therefore dV = 1 \times r \times r \sin \theta dr d\theta d\phi$$

$$= r^2 \sin \theta dr d\theta d\phi$$

(27)

Prove that

$$\nabla \times V = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} \bar{h}_1 & \bar{h}_2 & \bar{h}_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 v_1 & h_2 v_2 & h_3 v_3 \end{vmatrix}$$

We have

$$\nabla \times V = \nabla \times \left(\sum_i v_i \hat{e}_i \right) \text{ in cartesian}$$

$$= \nabla \times \left(\sum_P v_P \hat{e}_{(P)} \right) \text{ in o.c.c.}$$

Now taking components

$$\nabla \times \bar{v}_1 = \nabla \times (v_1 \hat{e}_{(1)})$$

$$= \nabla \times (v_1 h_1 \nabla q_1)$$

$$= \nabla(v_1 h_1) \times \nabla q_1 + v_1 h_1 \nabla \times \nabla q_1$$

$$= \nabla(v_1 h_1) \times \hat{e}_{(1)}$$

$$= \sum_i \left(\hat{e}_i \frac{\partial}{\partial q_i} (v_1 h_1) \right) \times \hat{e}_{(1)}$$

$$= \sum_i \frac{\hat{e}_i}{h_i} \frac{\partial}{\partial q_i} (v_1 h_1) \times \frac{\hat{e}_{(1)}}{h_1}$$

$$= \sum_i \frac{1}{h_i h_1} \frac{\partial}{\partial q_i} (v_1 h_1) (\hat{e}_{(i)} \times \hat{e}_{(1)})$$

On expanding, we get

$$\nabla \times \bar{v}_1 = \frac{1}{h_1 h_3} \frac{\partial}{\partial q_3} (v_1 h_1) \hat{e}_{(2)} - \frac{1}{h_1 h_2} \frac{\partial}{\partial q_2} (v_1 h_1) \hat{e}_{(3)}$$

$$= \frac{1}{h_1 h_2 h_3} \left[h_2 \frac{\partial}{\partial q_3} (v_1 h_1) \hat{e}_{(2)} - h_3 \frac{\partial}{\partial q_2} (v_1 h_1) \hat{e}_{(3)} \right]$$

similarly

$$\nabla \times \bar{v}_2 = \frac{1}{h_1 h_2 h_3} \left[h_3 \frac{\partial}{\partial q_1} (v_2 h_2) \hat{e}_{(3)} - h_1 \frac{\partial}{\partial q_3} (v_2 h_2) \hat{e}_{(1)} \right]$$

Adding together similar expression for $\nabla \cdot \bar{V}_3$
we get

$$\nabla \cdot \bar{V} = \begin{vmatrix} \bar{h}_1 & \bar{h}_2 & \bar{h}_3 \\ \frac{\partial}{\partial q_1} & \frac{\partial}{\partial q_2} & \frac{\partial}{\partial q_3} \\ h_1 v_1 & h_2 v_2 & h_3 v_3 \end{vmatrix} \quad \text{q.e.d.}$$

(28) Find an expression for $\nabla \psi$ in the parabolic co-ordinate system.

$$x_1 = uv \quad x_2 = \frac{1}{2}(u^2 - v^2) \quad x_3 = w.$$

We have

$$\nabla \psi = \sum_p \frac{\hat{e}_p}{h_p} \frac{\partial \psi}{\partial q_p}$$

$$h_1^2 = \sum_{i=1}^3 \left(\frac{\partial x_i}{\partial u} \right)^2 = v^2 + u^2 \Rightarrow h_1 = \sqrt{u^2 + v^2}$$

$$\text{Similarly, } h_2 = \sqrt{u^2 + v^2} \quad \& \quad h_3 = 1.$$

$$\therefore \nabla \psi = \frac{1}{(u^2 + v^2)^{1/2}} \frac{\partial \psi}{\partial u} \hat{e}_u + \frac{1}{(u^2 + v^2)^{1/2}} \frac{\partial \psi}{\partial v} \hat{e}_v + \frac{\partial \psi}{\partial w} \hat{e}_w$$

(29) Find an expression for $\nabla \cdot \bar{a}$ in parabolic co-ordinate system.

$$x_1 = uv, \quad x_2 = \frac{1}{2}(u^2 - v^2) \quad x_3 = w$$

We have

$$\nabla \cdot \bar{a} = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial (a_1 h_2 h_3)}{\partial q_1} + \frac{\partial (h_1 a_2 h_3)}{\partial q_2} + \frac{\partial (h_1 h_2 a_3)}{\partial q_3} \right]$$

As proved in the previous example

$$h_1 = h_2 = (u^2 + v^2)^{1/2}, \quad h_3 = 1$$

$$\therefore \nabla \cdot \bar{a} = \frac{1}{u^2 + v^2} \left[\frac{\partial}{\partial u} (u^2 + v^2)^{1/2} a_1 + \frac{\partial}{\partial v} (u^2 + v^2)^{1/2} a_2 + \frac{\partial (u^2 + v^2) a_3}{\partial w} \right]$$

$$= \frac{1}{u^2 + v^2} \left[\frac{\partial a_1 u}{\partial u} + \frac{\partial a_2 v}{\partial v} + (u^2 + v^2)^{1/2} \frac{\partial a_1}{\partial u} + \frac{2v a_2}{2(u^2 + v^2)^{1/2}} \right]$$

$$+ (u^2 + v^2)^{1/2} \frac{\partial a_2}{\partial v} + (u^2 + v^2) \frac{\partial a_3}{\partial w}$$

$$\therefore \nabla \cdot \bar{a} = \frac{1}{(u^2 + v^2)^{3/2}} [a_1 u + a_2 v] + \frac{1}{(u^2 + v^2)^{1/2}} \left[\frac{\partial a_1}{\partial u} + \frac{\partial a_2}{\partial v} + (u^2 + v^2)^{1/2} \frac{\partial a_3}{\partial w} \right]$$

(30) Using $\bar{V} = \nabla \psi$ derive the expression for $\nabla^2 \psi$ in curvilinear co-ordinates.

As we have already proved

$$\nabla \cdot \bar{V} = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial}{\partial q_1} (V_1 h_2 h_3) + \frac{\partial}{\partial q_2} (h_1 V_2 h_3) + \frac{\partial}{\partial q_3} (h_1 h_2 V_3) \right]$$

If $\bar{V} = \nabla \psi$, we have in O.C.C.

$$\underline{V}_1 = \frac{1}{h_1} \frac{\partial \psi}{\partial q_1}, \quad V_2 = \frac{1}{h_2} \frac{\partial \psi}{\partial q_2}, \quad V_3 = \frac{1}{h_3} \frac{\partial \psi}{\partial q_3}$$

Substituting

$$\nabla \cdot \bar{V} = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial}{\partial q_1} \left(\frac{h_2 h_3}{h_1} \frac{\partial \psi}{\partial q_1} \right) + \frac{\partial}{\partial q_2} \left(\frac{h_1 h_3}{h_2} \frac{\partial \psi}{\partial q_2} \right) + \frac{\partial}{\partial q_3} \left(\frac{h_1 h_2}{h_3} \frac{\partial \psi}{\partial q_3} \right) \right]$$

Since $\bar{V} = \nabla \psi$ we get $\nabla \cdot \bar{V} = \nabla^2 \psi$

$$\therefore \nabla^2 \psi = \frac{1}{h_1 h_2 h_3} \left[\frac{\partial}{\partial q_1} \left(\frac{h_2 h_3}{h_1} \frac{\partial \psi}{\partial q_1} \right) + \frac{\partial}{\partial q_2} \left(\frac{h_1 h_3}{h_2} \frac{\partial \psi}{\partial q_2} \right) + \frac{\partial}{\partial q_3} \left(\frac{h_1 h_2}{h_3} \frac{\partial \psi}{\partial q_3} \right) \right]$$

(31) If (r, θ, ϕ) are polar co-ordinates and $\psi(r, \theta, \phi)$ is a scalar pt. function, show that

$$\nabla^2 \psi = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2}$$

We have already obtained an expression for $\nabla^2 \psi$ in the previous problem, viz. (30)

Again, referring to problem (26) we have

$$h_r = 1, \quad h_\theta = r \quad \text{and} \quad h_\phi = r \sin \theta$$

Substituting these values and simplifying

$$\nabla^2 \psi = \frac{1}{r^2 \sin \theta} \left[\frac{\partial}{\partial r} \left(r^2 \sin \theta \frac{\partial \psi}{\partial r} \right) + \frac{\partial}{\partial \theta} \left(\frac{r \sin \theta}{r} \frac{\partial \psi}{\partial \theta} \right) + \frac{\partial}{\partial \phi} \left(\frac{r}{r \sin \theta} \frac{\partial \psi}{\partial \phi} \right) \right]$$

$$\therefore \nabla^2 \psi = \frac{1}{r^2 \sin \theta} \left[2r \sin \theta \frac{\partial \psi}{\partial r} + r^2 \sin \theta \frac{\partial^2 \psi}{\partial r^2} + \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{\sin \theta} \frac{\partial}{\partial \phi} \left(\frac{\partial \psi}{\partial \phi} \right) \right]$$

$$= \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial \psi}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \psi}{\partial \phi^2}$$

which is the required result.

(32) Show that $\psi = \frac{1}{r} e^{ikr}$ where k is a const. is a sdn. of the eqn.

$$\nabla^2 \psi + k^2 \psi = 0.$$

Since ψ is a fⁿ of r alone, we have

$$\nabla^2 \psi = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right)$$

$$\text{Now } \psi = \frac{1}{r} e^{ikr} \Rightarrow \frac{\partial \psi}{\partial r} = -\frac{e^{ikr}}{r^2} + \frac{ike^{ikr}}{r}$$

$$\therefore r^2 \frac{\partial \psi}{\partial r} = -e^{ikr} + rike^{ikr}$$

$$\therefore \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) = -ike^{ikr} + ike^{ikr} + r i^2 k^2 e^{ikr} \\ = -rk^2 e^{ikr} = -r^2 \frac{k^2 e^{ikr}}{r} = -r^2 k^2 \psi$$

$$\therefore \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial \psi}{\partial r} \right) = \frac{-r^2 k^2 \psi}{r^2} = -k^2 \psi$$

$$\therefore \nabla^2 \psi = -k^2 \psi$$

$$\therefore \nabla^2 \psi + k^2 \psi = 0$$

Thus, $\psi = \frac{1}{r} e^{ikr}$ satisfies the eqn. $\nabla^2 \psi + k^2 \psi = 0$ which is the required result.

(33) Using $\nabla q_1 = \hat{e}_{(1)}/h_1$ show that

$$\nabla \times \hat{e}_{(1)} = -\frac{\hat{e}_{(1)}}{h_1} \times \nabla h_1$$

$$\text{We have } \hat{e}_{(1)} = h_1 \nabla q_1$$

$$\begin{aligned} \therefore \nabla \times \hat{\underline{e}}_{(1)} &= \nabla \times (h_1 \nabla q_1) \\ &= \nabla h_1 \times \nabla q_1 + h_1 (\nabla \times \nabla q_1) \end{aligned}$$

but $\nabla \times \nabla q_1 = 0$.

$$\begin{aligned} \therefore \nabla \times \hat{\underline{e}}_{(1)} &= - \nabla q_1 \times \nabla h_1 \\ &= - \frac{\hat{\underline{e}}_{(1)}}{h_1} \times \nabla h_1 \end{aligned}$$

since $\nabla q_1 = \hat{\underline{e}}_{(1)} / h_1$,

$$\text{Thus } \nabla \times \hat{\underline{e}}_{(1)} = - \frac{\hat{\underline{e}}_{(1)}}{h_1} \times \nabla h_1 \quad \text{q.e.d.}$$

(34) Prove that

$$\sum_t h^{\lambda t} h_{tp} = \delta_p^\lambda$$

We have

$$\begin{aligned} h_p &= \sum_t h^t h_{pt} \\ \therefore h^\lambda \sum_t h^t h_{pt} &= \sum_t h^\lambda h^t h_{pt} = \sum_t h^{\lambda t} h_{pt} \end{aligned}$$

$$\therefore \sum_t h^{\lambda t} h_{pt} = h^\lambda \cdot h_p = \delta_p^\lambda$$

$$\therefore \sum_t h^{\lambda t} h_{pt} = \delta_p^\lambda \quad \text{q.e.d.}$$

(35) Use $h_{p\lambda} = \bar{h}_p \cdot \bar{h}_\lambda$ and $\bar{h}_p = \frac{\partial x}{\partial q_p}$

to show that

$$[p\lambda; t] = \bar{h}_t \cdot \frac{\partial \bar{h}_p}{\partial q_\lambda}$$

We have,

$$[p_{r:t}] = \frac{1}{2} \left[\frac{\partial \bar{h}_{pt}}{\partial p_r} + \frac{\partial \bar{h}_{rt}}{\partial p_r} - \frac{\partial \bar{h}_{pr}}{\partial p_r} \right]$$

$$= \frac{1}{2} \left[\frac{\partial}{\partial p_r} (\bar{h}_p \cdot \bar{h}_t) + \frac{\partial}{\partial p_r} (\bar{h}_r \cdot \bar{h}_t) - \frac{\partial}{\partial p_r} (\bar{h}_p \cdot \bar{h}_r) \right]$$

$$= \frac{1}{2} \left[\bar{h}_p \cdot \frac{\partial \bar{h}_t}{\partial p_r} + \bar{h}_t \cdot \frac{\partial \bar{h}_p}{\partial p_r} + \bar{h}_r \cdot \frac{\partial \bar{h}_t}{\partial p_r} + \bar{h}_t \cdot \frac{\partial \bar{h}_r}{\partial p_r} - \bar{h}_p \cdot \frac{\partial \bar{h}_r}{\partial p_r} - \bar{h}_r \cdot \frac{\partial \bar{h}_p}{\partial p_r} \right]$$

$$\text{Now } \frac{\partial \bar{h}_r}{\partial p_r} = \frac{\partial}{\partial p_r} \left(\frac{\partial \bar{x}}{\partial p_r} \right) = \frac{\partial}{\partial p_r} \left(\frac{\partial \bar{x}}{\partial p_r} \right) = \frac{\partial \bar{h}_t}{\partial p_r}$$

Hence, we get the only terms remaining as

$$2 [p_{r:t}] = \bar{h}_t \cdot \frac{\partial \bar{h}_p}{\partial p_r} \text{ and } \bar{h}_t \cdot \frac{\partial \bar{h}_r}{\partial p_r}$$

which are again equal.

Hence,

$$[p_{r:t}] = \frac{1}{2} [2 \bar{h}_t \cdot \frac{\partial \bar{h}_r}{\partial p_r}]$$

$$= \bar{h}_t \cdot \frac{\partial \bar{h}_r}{\partial p_r}$$

or again applying the result

$$[p_{r:t}] = \bar{h}_t \cdot \frac{\partial \bar{h}_p}{\partial p_r} \quad \text{q.e.d.}$$

(36) Prove that $\frac{\partial \bar{h}_j}{\partial a_k} = \sum_i [j k : i] \bar{h}^i$

We have, using the result of the previous problem,

$$\begin{aligned} \bar{h}_p \cdot \frac{\partial \bar{h}_j}{\partial a_k} &= [j k : p] \\ &= \sum_i [j k : i] \delta_p^i \\ &= \sum_i [j k : i] \bar{h}_p \cdot \bar{h}^i \\ &= \bar{h}_p \cdot \sum_i [j k : i] \bar{h}^i \end{aligned}$$

Hence

$$\frac{\partial \bar{h}_j}{\partial a_k} = \sum_i [j k : i] \bar{h}^i$$

(37) Show that

$$\frac{\partial \bar{h}_j}{\partial a_k} = \sum_l \{j^l k\} \bar{h}_l$$

We have $\sum_l \{j^l k\} \bar{h}_l = \sum_l \left[\sum_i [j k : i] h^{il} \right] \bar{h}_l$

$$= \sum_{li} [j k : i] h^{il} \bar{h}_l \quad \text{but } \sum_l h^{il} \bar{h}_l = \bar{h}^i$$

$$\therefore \frac{\partial \bar{h}_j}{\partial a_k} = \sum_i [j k : i] \bar{h}^i$$

but we have, by problem (36)

$$\sum_i [j k : i] \bar{h}^i = \frac{\partial \bar{h}_j}{\partial a_k}$$

$$\therefore \sum_l \{j^l k\} \bar{h}_l = \frac{\partial \bar{h}_j}{\partial a_k} \quad \text{q.e.d.}$$

(38) Prove that the value of a determinant is unaltered if to

(38) Show that

$$\sum_i \sum_k \{i^i k\} = \frac{1}{2} \frac{\partial \ln h}{\partial q_k}$$

$$\begin{aligned} \text{We have } \{j^i k\} &= \sum_p h^{ip} [jk \cdot p] \\ &= \frac{1}{2} \sum_p h^{ip} \left[\frac{\partial h_{pj}}{\partial q_k} + \frac{\partial h_{kp}}{\partial q_j} - \frac{\partial h_{jk}}{\partial q_p} \right] \end{aligned}$$

~~$\{j^i k\}$~~

$$\begin{aligned} \therefore \{i^i k\} &= \frac{1}{2} \sum_{i,p} h^{ip} \left[\frac{\partial h_{pi}}{\partial q_k} + \frac{\partial h_{kp}}{\partial q_i} - \frac{\partial h_{ik}}{\partial q_p} \right] \\ &= \frac{1}{2} \sum_{i,p} h^{ip} \left[\frac{\partial h_{pi}}{\partial q_k} + \frac{\partial h_{kp}}{\partial q_i} - \frac{\partial h_{kp}}{\partial q_i} \right] \end{aligned}$$

As interchange of i & p is permitted in the last term.

$$\therefore \{i^i k\} = \frac{1}{2} \sum_{i,p} h^{ip} \frac{\partial h_{ip}}{\partial q_k}$$

we have $h^{ip} = \delta_{ip} / h_i^2$

$$\therefore \{i^i k\} = \frac{1}{2} \sum_i \frac{1}{h_i^2} \frac{\partial h_{ii}}{\partial q_k}$$

$$= \frac{1}{2} \frac{1}{h} \frac{\partial h}{\partial q_k}$$

On summing up.
as $h = h_1^2 h_2^2 h_3^2$

$$= \frac{1}{2} \frac{\partial \ln h}{\partial q_k}$$

$$\therefore \{i^i k\} = \frac{1}{2} \frac{\partial \ln h}{\partial q_k} \quad \text{q.e.d.}$$

$$(39) \text{ If } B_i = \sum_{jk} \epsilon_{ijk} \frac{\partial A_j}{\partial q_k}$$

$$\text{Show that } \sum_k \epsilon_{ijk} B_k = \frac{\partial A_i}{\partial q_j} - \frac{\partial A_j}{\partial q_i}$$

Now, we have

$$B_k = \sum_{lm} \epsilon_{klm} \frac{\partial A_l}{\partial q_m}$$

$$\therefore \sum_k \epsilon_{ijk} B_k = \sum_{klm} \epsilon_{klm} \frac{\partial A_l}{\partial q_m} \epsilon_{ijk}$$

$$= \sum_{lm} \frac{\partial A_l}{\partial q_m} \left(\sum_k \epsilon_{ijk} \epsilon_{klm} \right)$$

$$= \sum_{lm} \frac{\partial A_l}{\partial q_m} (\delta_{li} \delta_{mj} - \delta_{lj} \delta_{mi})$$

$$= \sum_{lm} \frac{\partial A_l}{\partial q_m} \delta_{li} \delta_{mj} - \sum_{lm} \delta_{lj} \delta_{mi} \frac{\partial A_l}{\partial q_m}$$

$$\text{Thus } \sum_k \epsilon_{ijk} B_k = \frac{\partial A_i}{\partial q_j} - \frac{\partial A_j}{\partial q_i} \quad \text{q.e.d.}$$

(40) Representing the second rank covariant tensor

by $h_{ij} = h_i h_j$, show that

$$h_{ij,k} = \frac{\partial h_{ij}}{\partial q_k} - \sum_l \{i^l k\} h_{lj} - \sum_l \{j^l k\} h_{il}$$

hence deduce the result $h_{ij,k} = 0$.

Now, we already have

$$h_{i,k} = \frac{\partial h_i}{\partial q_k} - \sum_l \{i^l k\} h_l$$

And since $h_{ij} = h_i h_j$

$$\therefore h_{ij,k} = h_{i,k} h_j + h_i h_{j,k}$$

$$\therefore h_{ij,k} = h_j \left\{ \frac{\partial h_i}{\partial q_k} - \sum_l \{i^l_k\} h_{le} \right\} + h_i \left\{ \frac{\partial h_j}{\partial q_k} - \sum_l \{j^l_k\} h_{le} \right\}$$

$$= h_j \frac{\partial h_i}{\partial q_k} + h_i \frac{\partial h_j}{\partial q_k} - \sum_l \{i^l_k\} h_{lj} - \sum_l \{j^l_k\} h_{il}$$

~~the terms cancel.~~

$$\therefore h_{ij,k} = \frac{\partial h_{ij}}{\partial q_k} - \sum_l \{i^l_k\} h_{lj} - \sum_l \{j^l_k\} h_{il}$$

which is the required result.

Now

$$\{i^l_k\} = \sum_p [i_k:p] h^{pl}$$

$$\therefore \sum_l \{i^l_k\} h_{lj} = \sum_{p,l} [i_k:p] h^{pl} h_{lj}$$

$$= \sum_p [i_k:p] \delta_j^p = [i_k:j]$$

Similarly, we get $\sum_l \{j^l_k\} h_{il} = [j_k:i]$

Now we have

$$[i_k:j] = h_j \frac{\partial h_i}{\partial q_k} \quad \& \quad [j_k:i] = h_i \frac{\partial h_j}{\partial q_k}$$

$$\therefore h_{ij,k} = h_j \frac{\partial h_i}{\partial q_k} + h_i \frac{\partial h_j}{\partial q_k} - h_j \frac{\partial h_i}{\partial q_k} - h_i \frac{\partial h_j}{\partial q_k}$$

$$\therefore h_{ij,k} = 0 \quad \text{q.e.d.}$$

(41) If any two rows of a determinant are proportional, then the determinant vanishes.

Let the l^{th} row be k times the m^{th} row
we have

$$\begin{aligned} D_n &= \sum_p d_p P [a_{11} \dots a_{ll} \dots a_{mm} \dots a_{nn}] \\ &= \sum_p d_p P [a_{11} \dots k a_{mm} \dots a_{mm} \dots a_{nn}] \\ &= k D_n' \quad \text{where } D_n' = \sum_p d_p P [a_{11} \dots a_{mm} \dots a_{nn}] \end{aligned}$$

since, if two rows of a determinant are equal then its value is zero,

we have $D_n' = 0$.

$$\therefore D_n = k D_n' = 0 \quad \text{q.e.d.}$$

(42) The value of a determinant is unchanged if ~~to~~ to each element of any row is added k times the corresponding element of some other row, where k is a const.

$$\text{Let } D_n = \sum_p d_p P [a_{11} \dots a_{ii} \dots a_{jj} \dots a_{nn}]$$

$$\begin{aligned} \text{Let } D_n' &= \sum_p d_p P [a_{11} \dots a_{ii} + k a_{jj} \dots a_{jj} \dots a_{nn}] \\ &= \sum_p d_p P [a_{11} \dots a_{nn}] + k \sum_p d_p P [a_{11} \dots a_{jj} a_{jj} a_{nn}] \\ &= D_n + 0 \end{aligned}$$

$$\therefore D_n' = D_n \quad \text{q.e.d.}$$

(43) Given that \bar{B} is a vector and C_{ij} are the components of a second rank tensor and that $\sum A_{ijk} B^k = C_{ij}$ holds in all frames of reference

show that A_{ijk} is a third rank tensor. Assume that B is independent of A_{ijk}

Now, we have

Since $\sum_k A_{ijk} B^k = C_{ij}$ holds in all frames

$$\therefore \sum_n A'_{lmn} B'^n = C'_{lm}$$

$$\text{Now } C'_{lm} = \sum_n A'_{lmn} B'^n \\ = \sum_{ij} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} C_{ij}$$

$$= \sum_{ij} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} \sum_k A_{ijk} B^k$$

As B^k is independent of A_{ijk} , $B^k = \sum_n \frac{\partial q_k}{\partial q'^n} B'^n$
since B^k are contravariant components.

$$\therefore C'_{lm} = \sum_{ijk} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} A_{ijk} \sum_n \frac{\partial q_k}{\partial q'^n} B'^n$$

$$\therefore \sum_n A'_{lmn} B'^n = \sum_n \sum_{ijk} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} \frac{\partial q_k}{\partial q'^n} A_{ijk} B'^n$$

$$\therefore \sum_n \left[A'_{lmn} - \sum_{ijk} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} \frac{\partial q_k}{\partial q'^n} A_{ijk} \right] B'^n = 0$$

$$\therefore \cancel{A'}_{lmn} = \sum_{ijk} \frac{\partial q_i}{\partial q'^l} \frac{\partial q_j}{\partial q'^m} \frac{\partial q_k}{\partial q'^n} A_{ijk}$$

which is according to the law for transformations of the covariant components of a tensor of rank 3.

$\therefore A_{ijk}$ is a covariant tensor of rank 3 q.e.d.

(44) $\sum_{ij} K_{ij} A^i B^j$ is invariant for any two vectors A^i, B^j prove that K_{ij} is a second rank covariant tensor.
 Now, ~~but~~ since we have

$$\sum_{ij} K_{ij} A^i B^j \text{ invariant}$$

$$\therefore \sum_{p' r'} K'_{p' r'} A'^{p'} B'^{r'} = \sum_{ij} K_{ij} A^i B^j$$

since A^i & B^j are contravariant vectors,

$$A^i = \sum_p \frac{\partial q_i}{\partial q'^p} A'^p \quad B^j = \sum_{r'} \frac{\partial q_j}{\partial q'^{r'}} B'^{r'}$$

$$\therefore \sum_{p' r'} K'_{p' r'} A'^{p'} B'^{r'} = \sum_{ij p' r'} K_{ij} \frac{\partial q_i}{\partial q'^{p'}} \frac{\partial q_j}{\partial q'^{r'}} A'^{p'} B'^{r'}$$

$$\therefore \sum_{p' r'} A'^{p'} B'^{r'} \left[K'_{p' r'} - \sum_{ij} \frac{\partial q_i}{\partial q'^{p'}} \frac{\partial q_j}{\partial q'^{r'}} K_{ij} \right] = 0$$

$$\therefore K'_{p' r'} = \sum_{ij} \frac{\partial q_i}{\partial q'^{p'}} \frac{\partial q_j}{\partial q'^{r'}} K_{ij}$$

which is the transformation law for second rank covariant tensor.

$\therefore K_{ij}$ is a second rank covariant tensor. q.e.d.

(45) If $T_{ij \dots n}$ is a tensor of rank n , then show that $\sum_j \frac{\partial}{\partial x_j} (T_{ij \dots n})$ is a tensor of rank $n-1$.

We have, since $T_{ij \dots n}$ is an n^{th} rank tensor

$$T'_{\alpha \beta \dots \eta} = \sum_{ijk \dots n} \frac{\partial x'_\alpha}{\partial x_i} \frac{\partial x'_\beta}{\partial x_j} \dots \frac{\partial x'_\eta}{\partial x_n} T_{ijk \dots n}$$

$$\begin{aligned} \therefore \sum_{\beta} \frac{\partial T_{\alpha\beta\dots n}}{\partial x^{\beta}} &= \sum_{ij\dots n} \frac{\partial x^i}{\partial x^{\beta}} \dots \frac{\partial T_{i\dots n}}{\partial x^{\beta}} \\ &= \sum_{i\dots n} \frac{\partial x^i}{\partial x^{\beta}} \frac{\partial x^{\beta}}{\partial x^i} \dots \frac{\partial T_{i\dots n}}{\partial x^i} \\ &= \sum_{i\dots n} \frac{\partial x^i}{\partial x^i} \dots \frac{\partial T_{i\dots n}}{\partial x^i} \\ &= \sum_{i\dots n} \frac{\partial T_{i\dots n}}{\partial x^i} \end{aligned}$$

$$\therefore \sum_{\beta} \frac{\partial T'_{\alpha\beta\dots n}}{\partial x'^{\beta}} = \sum_{i\dots n} \frac{\partial x^i}{\partial x'^{\beta}} \left(\sum_j \frac{\partial T}{\partial x^j} \right)$$

Which is the transformation law for tensors of rank $n-1$.

Hence $\sum_j \frac{\partial T_{i\dots n}}{\partial x^j}$ is a tensor of rank $n-1$.

46 Show that, a negative scalar field is connected to the negative vector.

Now, we have to prove that

$$(-1)\bar{u} = -\bar{u}$$

we have

$$(-1) + 1 = 0$$

$$\therefore [(-1) + 1] \bar{u} = 0 \bar{u} = 0$$

$$\therefore (-1)\bar{u} + \bar{u} = 0$$

$$\therefore (-1)\bar{u} = -\bar{u} \quad \text{q.e.d.}$$

47) Show that a set of n tuples of complex no.s forms a vector space over a field of complex no.s.

$$u = (u_1, \dots, u_n) \quad v = (v_1, \dots, v_n)$$

$$\bar{u} + \bar{v} = (u_1 + v_1, \dots, u_n + v_n) \quad a(\bar{u}) = (au_1, \dots, au_n)$$

Now

Since closure under addition holds for complex no.s, it also holds for this set.

Since for every u, v, \exists unique $u+v$, for every $\bar{u}, \bar{v} \exists$ unique $\bar{u} + \bar{v}$.

$$(u_1 + v_1) + w_1 = u_1 + (v_1 + w_1) \text{ for complex no.s}$$

$$\Rightarrow (\bar{u} + \bar{v}) + \bar{w} = \bar{u} + (\bar{v} + \bar{w}) \text{ holds for the above set.}$$

$$\text{Similarly } u_1 + v_1 = v_1 + u_1 \Rightarrow \bar{u} + \bar{v} = \bar{v} + \bar{u}.$$

$$\exists 0 = (0, \dots, 0) \text{ s.t. } \bar{u} + \bar{0} = \bar{0} + \bar{u} = \bar{u}$$

$$\exists -\bar{v} = (-v_1, -v_2, \dots, -v_n) \text{ for every } \bar{v} \text{ s.t. } \bar{v} + (-\bar{v}) = 0.$$

Since closure under multiplication holds for complex no.s, it also holds for the above set.

Similarly commutativity under scalar multiplication follows along with associativity also.

$$\exists 0 \text{ s.t. } 0(\bar{u}) = 0.$$

Thus, all the postulates for a vector space are satisfied by the set of n -tuples of complex no.s.

\therefore It is a vector space.

(48) If the spaces l_1, \dots, l_n are linearly independent, show that every vector X contained in l_1, \dots, l_n can be written uniquely as

$$\bar{X} = \sum x_i \quad \text{where } \bar{x}_i \in l_i$$

Now, we have

$$\bar{X} = \sum_i x_i = \sum_i \bar{x}'_i \quad (\text{say})$$

$$\therefore \bar{X} - \bar{X} = 0 = \sum_i (x_i - \bar{x}'_i)$$

$$x_i, \bar{x}'_i \in l_i \Rightarrow \bar{x}_i - \bar{x}'_i \in l_i$$

Hence $\bar{x}_i - \bar{x}'_i = 0 \Rightarrow x_i - \bar{x}'_i = 0$ for every component separately. [due to linear independence.]

$$\therefore x_i = \bar{x}'_i$$

\therefore The representation $\sum_i x_i = \bar{X}$ is unique.

(49) Show that the two dimensional subspace L_2 of E_3 is a proper subspace.

Now, we have

in E_3 , basis vectors i, j, k .

We consider L_2 with a basis i, j .

Now orthogonality of $i, j, k \Rightarrow L_2$ is closed under all the operations on i, j .

Similarly ~~L_2~~ since i, j are the basis vectors all the properties of a vector space viz.

associativity & commutativity under addition and scalar multiplication hold.

$$\exists \vec{0} = 0\hat{i} + 0\hat{j} \text{ s.t. } \vec{0} + \vec{v} = \vec{v}$$

$$\exists \vec{0} \text{ s.t. } 0\vec{v} = \vec{0}. \quad \exists -\vec{v} = -v_1\hat{i} + -v_2\hat{j}$$

Hence L_2 is a vector space.

$$\text{Now } \hat{k} \notin L_2, \hat{i}, \hat{j} \in E_3$$

$\therefore L_2$ is a proper subspace of E_3 .

(50) Are the vectors

$\bar{x}_1 = (0, -1, 0)$, $\bar{x}_2 = (0, 1, -1)$ & $\bar{x}_3 = (1, -2, 1)$ linearly independent? Express $(-2, 1, -3) = \bar{x}$ as a combination (linear) of $\bar{x}_1, \bar{x}_2, \bar{x}_3$ if possible.

Now, consider

$$a\bar{x}_1 + b\bar{x}_2 + c\bar{x}_3 = \vec{0}$$

\therefore Considering the components.

$$0a + 0b + c = 0 \Rightarrow c = 0$$

$$-a + b - 2c = 0 \Rightarrow -a + b = 0 \Rightarrow a = b$$

$$0a - 0b + c = 0 \Rightarrow -b = 0 \Rightarrow b = 0 \Rightarrow a = 0$$

$$\text{Thus } a\bar{x}_1 + b\bar{x}_2 + c\bar{x}_3 = \vec{0} \Rightarrow a = b = c = 0$$

$\therefore \bar{x}_1, \bar{x}_2, \bar{x}_3$ are linearly independent.

$$\text{Let } \bar{x} = m\bar{x}_1 + n\bar{x}_2 + p\bar{x}_3$$

$$\therefore 0m + 0n + p = -2 \Rightarrow p = -2$$

$$-m + n - 2p = 1 \Rightarrow n - m = -3$$

$$0m - n + p = -3 \Rightarrow -n = -1 \Rightarrow n = 1 \Rightarrow m = 4$$

$$\therefore \bar{x} = 4\bar{x}_1 + \bar{x}_2 - 2\bar{x}_3$$

(51) Using $(u, v) = (vU)^*$, $(au, v) = a^*(u, v)$
show that $(u, av) = a(uv)$

We have

$$\begin{aligned}(u, av) &= (av, u)^* = \{a^*(vU)\}^* \\ &= a(vU)^* = a(uv) \quad \text{q.e.d.}\end{aligned}$$

(52) Prove that $(u+v, w) = (u, w) + (v, w)$

Now we have

$$\begin{aligned}(u+v, w) &= (w, u+v)^* \\ &= [(w, u) + (w, v)]^* \\ &= (wU)^* + (wV)^* \\ &= (uW) + (vW) \quad \text{q.e.d.}\end{aligned}$$

(53) Prove that $\|a\bar{v}\| = |a| \|v\|$

We have

$$\begin{aligned}\|a\bar{v}\| &= \sqrt{(a\bar{v}, a\bar{v})} \\ &= \sqrt{a(a\bar{v}, \bar{v})} \\ &= \sqrt{aa^*(\bar{v}, \bar{v})} \\ &= \sqrt{|a|^2 \|v\|^2}\end{aligned}$$

$$\therefore \|a\bar{v}\| = |a| \|v\| \quad \text{q.e.d.}$$

(54) Prove Schwartz's inequality

$$|(\bar{u} \bar{v})| \leq \|\bar{u}\| \|\bar{v}\|$$

Now, consider $\bar{w} = \bar{u} - a\bar{v}$ $a = \frac{(\bar{v} \bar{u})}{(\bar{v} \bar{v})}$

$$0 \leq (\bar{w} \bar{w})$$

$$\therefore 0 \leq (\bar{u} - a\bar{v}, \bar{u} - a\bar{v})$$

$$\therefore 0 \leq (\bar{u} \bar{u}) - (\bar{u} a\bar{v}) - (a\bar{v} \bar{u}) + (a\bar{v} a\bar{v})$$

$$\therefore 0 \leq (\bar{u}, \bar{u}) - a(\bar{u} \bar{v}) - a^*(\bar{v} \bar{u}) + aa^*(\bar{v} \bar{v})$$

Substituting the value of a

$$0 \leq (\bar{u} \bar{u}) - \frac{(\bar{v} \bar{u})(\bar{u} \bar{v})}{(\bar{v} \bar{v})} - \frac{(\bar{u} \bar{v})(\bar{v} \bar{u})}{(\bar{v} \bar{v})} + \frac{(\bar{u} \bar{v})(\bar{v} \bar{u})}{(\bar{v} \bar{v})}$$

$$\therefore 0 \leq (\bar{u} \bar{u})(\bar{v} \bar{v}) - (\bar{u} \bar{v})(\bar{v} \bar{u})$$

$$\therefore (\bar{v} \bar{u})(\bar{u} \bar{v}) \leq (\bar{u} \bar{u})(\bar{v} \bar{v})$$

$$\therefore |(\bar{u} \bar{v})|^2 \leq \|\bar{u}\|^2 \|\bar{v}\|^2$$

$$\therefore |(\bar{u} \bar{v})| \leq \|\bar{u}\| \|\bar{v}\| \quad \text{q.e.d.}$$

~~(55) Prove triangle inequality~~

~~$$\|\bar{u} + \bar{v}\| \leq \|\bar{u}\| + \|\bar{v}\|$$~~

~~Now we have~~

~~$$\|\bar{u} + \bar{v}\|^2 = (\bar{u} + \bar{v}, \bar{u} + \bar{v})$$~~

~~$$= (\bar{u} \bar{u}) + (\bar{u} \bar{v}) + (\bar{v} \bar{u}) + (\bar{v} \bar{v})$$~~

~~$$= \|\bar{u}\|^2 + |(\bar{u} \bar{v})|^2 + \|\bar{v}\|^2$$~~

(55) Show that the n dimensional complex vector space satisfies the usual rules regarding the scalar product.

$$\begin{aligned} \text{We have } (\bar{u} \bar{v}) &= \sum_{i,j} (u_i^* \hat{e}_{(i)}) \cdot (v_j \hat{e}_{(j)}) \\ &= \sum_{i,j} u_i^* v_j \delta_{ij} \\ &= \sum_i u_i^* v_i \end{aligned}$$

Now we see

$$\begin{aligned} \text{(i) } (\bar{v} \bar{u}) &= \sum_i v_i^* u_i \\ &= \sum_i (v_i u_i^*)^* \\ &= \sum_i (u_i^* v_i)^* \\ &= (\bar{u} \bar{v})^* \\ \therefore (\bar{v} \bar{u}) &= (\bar{u} \bar{v})^* \end{aligned}$$

$$\begin{aligned} \text{(ii) } (\bar{u}, \bar{v} + \bar{w}) &= \sum_i u_i^* (v_i + w_i) \\ &= \sum_i u_i^* v_i + \sum_i u_i^* w_i \end{aligned}$$

$$\therefore (\bar{u} \bar{v} + \bar{w}) = (\bar{u} \bar{v}) + (\bar{u} \bar{w})$$

$$\begin{aligned} \text{(iii) } (a \bar{u} \bar{v}) &= \sum_i (a u_i^*) v_i \\ &= \sum_i a^* u_i^* v_i = a^* \sum_i u_i^* v_i \\ &= a^* (\bar{u} \bar{v}) \end{aligned}$$

Thus the scalar product as defined above satisfies the usual rules.

56) Express Schwartz's inequality in terms of the components of the complex vector space C_n

We have Schwartz's inequality as

$$|(\bar{u} \bar{v})| \leq \|\bar{u}\| \|\bar{v}\|$$

Hence for C_n

$$|(\bar{u} \bar{v})| = \left| \sum_i u_i^* v_i \right|$$

$$\& \|\bar{u}\| = \sqrt{|(\bar{u} \bar{u})|} = \sqrt{\sum_i u_i^* u_i}$$

$$\therefore \left| \sum_i u_i^* v_i \right| \leq \sqrt{\sum_i u_i^* u_i} \sqrt{\sum_i v_i^* v_i}$$

57) Express the triangle inequality in terms of the components of C_n .

We have

$$\|\bar{u} + \bar{v}\| \leq \|\bar{u}\| + \|\bar{v}\|$$

We have

$$\|\bar{u} + \bar{v}\| = \sqrt{(\bar{u} + \bar{v})(\bar{u} + \bar{v})} = \sqrt{\sum_{ij} (u_i^* + v_j^*)(u_i + v_j)}$$

$$\|\bar{u}\| = \sqrt{\sum_i u_i^* u_i}$$

$$\therefore \sqrt{\sum_{ij} (u_i^* + v_j^*)(u_i + v_j)} \leq \sqrt{\sum_i u_i^* u_i} + \sqrt{\sum_j v_j^* v_j}$$

(58) If f and g are bounded then f^*g and fg^* are also bounded. Prove this. Also prove that $|f+g|$ exists in the same space.

Consider $|f+g|^2$

$$|f+g|^2 = |f|^2 + |g|^2 + |(f^*g)| + |(fg^*)|$$

Now, we have

$$|(fg^*)| \leq |f| |g^*|$$

$$\therefore |(fg^*)| \leq |f| |g| \quad \text{since } |g^*| = |g|$$

$\therefore fg^*$ is bounded, as ~~f and g~~ f & g are bounded.

Similarly f^*g is also bounded.

Hence the RHS of

$$|f+g|^2 = |f|^2 + |g|^2 + |(f^*g)| + |(fg^*)|$$

is bounded

$\therefore f+g$ is also bounded.

$\therefore |f+g|$ belongs to the same space.

(59) Prove that

$$\|\bar{u} + \bar{v}\|^2 + \|\bar{u} - \bar{v}\|^2 = 2\|\bar{u}\|^2 + 2\|\bar{v}\|^2$$

we have

$$\|\bar{u} + \bar{v}\|^2 = (\bar{u} + \bar{v}, \bar{u} + \bar{v}) = (\bar{u}\bar{u}) + (\bar{u}\bar{v}) + (\bar{v}\bar{u}) + (\bar{v}\bar{v})$$

$$\|\bar{u} - \bar{v}\|^2 = (\bar{u} - \bar{v}, \bar{u} - \bar{v}) = (\bar{u}\bar{u}) - (\bar{u}\bar{v}) - (\bar{v}\bar{u}) + (\bar{v}\bar{v})$$

Adding

$$\|\bar{u} + \bar{v}\|^2 + \|\bar{u} - \bar{v}\|^2 = 2\|\bar{u}\|^2 + 2\|\bar{v}\|^2 \quad \text{q.e.d.}$$

(60) Prove the Pythagoras theorem

i.e. $\|\bar{u} - \bar{v}\|^2 = \|\bar{u}\|^2 + \|\bar{v}\|^2$ if $(\bar{u}, \bar{v}) = 0$.

Now

$$\begin{aligned}\|\bar{u} - \bar{v}\|^2 &= (\bar{u} - \bar{v}, \bar{u} - \bar{v}) = (\bar{u}\bar{u}) - (\bar{u}\bar{v}) - (\bar{v}\bar{u}) + (\bar{v}\bar{v}) \\ &= (\bar{u}\bar{u}) - (\bar{u}\bar{v}) - (\bar{v}\bar{u}) + (\bar{v}\bar{v})\end{aligned}$$

$$(\bar{u}\bar{v}) = 0 \Rightarrow (\bar{v}\bar{u}) = (\bar{u}\bar{v})^* = 0.$$

$$\therefore \|\bar{u} - \bar{v}\|^2 = \|\bar{u}\|^2 + \|\bar{v}\|^2 \quad \text{q.e.d.}$$

(61) In Gram Schmidt Process of orthonormalization

we have

$$\bar{x}_k = \frac{d_k}{\|d_k\|} \quad \text{where } d_k = \begin{pmatrix} (\bar{y}_1, \bar{y}_1) & \dots & (\bar{y}_1, \bar{y}_k) \\ \vdots & \ddots & \vdots \\ (\bar{y}_k, \bar{y}_k - \bar{y}_1) & \dots & \bar{y}_k \end{pmatrix}$$

Verify this for $k=1$ & 2

(a) For $k=1$

$$\bar{x}_1 = \frac{\bar{y}_1}{\|\bar{y}_1\|} \quad \text{which is obviously true}$$

& consistent with the previous results of G.S.O process

(b) for $k=2$

$$\bar{x}_2 = \frac{\begin{vmatrix} (\bar{y}_1, \bar{y}_1) & (\bar{y}_1, \bar{y}_2) \\ \bar{y}_1 & \bar{y}_2 \end{vmatrix}}{\| \begin{vmatrix} (\bar{y}_1, \bar{y}_1) & (\bar{y}_1, \bar{y}_2) \\ \bar{y}_1 & \bar{y}_2 \end{vmatrix} \|} = \frac{\bar{y}_2 (\bar{y}_1, \bar{y}_1) - \bar{y}_1 (\bar{y}_1, \bar{y}_2)}{\| \bar{y}_2 (\bar{y}_1, \bar{y}_1) - \bar{y}_1 (\bar{y}_1, \bar{y}_2) \|}$$

$$\therefore \bar{x}_2 = \frac{\bar{y}_2 - \frac{\bar{y}_1 (\bar{y}_1, \bar{y}_2)}{(\bar{y}_1, \bar{y}_1)}}{\| \bar{y}_2 - \frac{\bar{y}_1 (\bar{y}_1, \bar{y}_2)}{(\bar{y}_1, \bar{y}_1)} \|} = \frac{\bar{y}_2 - (\bar{y}_1, \bar{y}_2) \bar{x}_1}{\| \bar{y}_2 - (\bar{y}_1, \bar{y}_2) \bar{x}_1 \|} \quad \text{q.e.d.}$$

62) Starting from the linearly independent square integrable polynomial basis

$1, x, x^2, \dots, x^n$ defined on the interval -1 to $+1$ deduce an orthonormal basis.

Now let the basis be

$$\psi_0 \dots \psi_{n-1}$$

Now we have

$$\psi_0 = \frac{1}{\|1\|} \quad \text{But we have}$$

$$\|f\|^2 = \int_{-1}^1 |f|^2 dx \quad \therefore \|1\|^2 = [1 - (-1)] = 2$$

$$\|1\| = \sqrt{2}$$

$$\psi_0 = \frac{1}{\sqrt{2}}$$

Now going to ψ_1 , we have

$$\psi_1 = \frac{d_2}{\|d_2\|} \quad \text{where } d_2 = \begin{vmatrix} (1 \ 1) & (1 \ x) \\ 1 & x \end{vmatrix}$$

$$\therefore d_2 = 2x$$

$$\therefore \|d_2\|^2 = \int_{-1}^1 4x^2 dx = \left[\frac{4x^3}{3} \right]_{-1}^1 = \frac{8}{3}$$

$$\therefore \|d_2\| = \sqrt{8/3}$$

$$\therefore \psi_1 = \frac{2x}{\sqrt{8/3}} = \frac{\sqrt{3}}{2} x$$

Proceeding along similar lines, we can find

$$\psi_3 \dots \psi_n$$

(63) Test these vectors for linear independence.

$$x_1 = \begin{bmatrix} 1 \\ 0 \\ 1 \\ 0 \end{bmatrix} \quad x_2 = \begin{bmatrix} 1 \\ -1 \\ 0 \\ 1 \end{bmatrix} \quad x_3 = \begin{bmatrix} 0 \\ 1 \\ -1 \\ 1 \end{bmatrix} \quad x_4 = \begin{bmatrix} 1 \\ -1 \\ 1 \\ -1 \end{bmatrix}$$

Consider $\sum c_i x_i = 0$

$$\therefore c_1 + c_2 + c_4 = 0$$

$$-c_2 + c_3 - c_4 = 0$$

$$c_1 - c_3 + c_4 = 0$$

$$c_2 + c_3 - c_4 = 0$$

Now For c_1, c_2, c_3, c_4 to have nonzero solns

$$\begin{vmatrix} 1 & 1 & 0 & -1 \\ 0 & -1 & 1 & -1 \\ 1 & 0 & -1 & 1 \\ 0 & 1 & 1 & -1 \end{vmatrix} \text{ must be equal to zero.}$$

but this is equal to -2 .

$$\therefore c_1 = c_2 = c_3 = c_4 = 0.$$

Thus

$$\sum c_i x_i = 0 \Rightarrow \text{all } c_i = 0.$$

\therefore The vectors are linearly independent.

(64) Consider two sets of rectangular co-ord for $E=2$ space with common origin unit vectors being along the co-ord. axes. In terms of cosines of the angles between the two sets of axes, find

the matrix A relating the two co-ord systems.

Now, we have

If the axes turn at an angle θ .

$$x' = x \cos \theta + y \sin \theta$$

$$y' = -x \sin \theta + y \cos \theta.$$

$$\therefore \begin{bmatrix} x' \\ y' \end{bmatrix} = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix}$$

$A = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}$ gives the transformation matrix.

And, rotating through $(-\theta)$

$$A^{-1} = \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix}$$

$$\text{but } A^+ = \begin{bmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{bmatrix}$$

$$\therefore A^+ = A^{-1}$$

$\therefore A$ is orthogonal.

(65) Given two basis $\sum x_i$, $\sum y_i$ such that $x_i = \sum_j a_{ij} y_j$ prove that the transformation matrix is nonsingular.

Now, since $\sum x_i$, $\sum y_i$ are both basis,

we can have

$$Y_k = \sum_l b_{kl} X_l.$$

$$\therefore X_i = \sum_j a_{ij} Y_j = \sum_j a_{ij} \left[\sum_l b_{jl} X_l \right]$$

$$\therefore X_i = \sum_{j,l} a_{ij} b_{jl} X_l.$$

but linear independence gives

$$X_i = \sum_l X_l d_{il} \quad \sum_l X_l d_{il}$$

$$\therefore \sum_l \cancel{X_l} d_{il} X_l = \sum_{j,l} \cancel{X_l} a_{ij} b_{jl} X_l.$$

$$\therefore \sum_l [d_{il} - \sum_j a_{ij} b_{jl}] X_l = 0.$$

$$\therefore \sum_j a_{ij} b_{jl} = d_{il}.$$

$$\therefore \sum_j a_{ij} b_{jl} = I$$

$$\therefore AB = I$$

This shows that ~~the~~ A can not be a singular matrix.

$$\therefore A^{-1} = B.$$

$$\therefore \{x_i\} = A \{y_i\} \quad \{y_i\} = A^{-1} \{x_i\}$$

which give the transformation relations.

66) Find $C_i, i=1, \dots, m$ which minimises
 $\| \bar{U} - \sum_{i=1}^m (C_i X_i) \|^2$ where \bar{U} is a given vector
 in an n dimensional vector space and X_i
 is a set of orthonormal vectors.

~~When~~ Now, we have

$$0 \leq \| \bar{U} - \sum_{i=1}^m C_i \bar{X}_i \|^2$$

$$= (\bar{U} - \sum_{i=1}^m C_i \bar{X}_i, \bar{U} - \sum_{j=1}^m C_j \bar{X}_j)$$

$$= (\bar{U}, \bar{U}) - (\bar{U}, \sum_{j=1}^m C_j \bar{X}_j) - (\sum_{i=1}^m C_i \bar{X}_i, \bar{U}) + (\sum_{i=1}^m C_i \bar{X}_i, \sum_{j=1}^m C_j \bar{X}_j)$$

$$= \| \bar{U} \|^2 - \sum_j C_j (\bar{U}, \bar{X}_j) - \sum_j C_j^* (\bar{X}_j, \bar{U}) + \sum_{i,j} C_i^* C_j (\bar{X}_i, \bar{X}_j)$$

Adding and subtracting $\sum_{i=1}^m |C_i - (\bar{X}_i, \bar{U})|^2$ gives

$$0 \leq \| \bar{U} \|^2 - \sum_{i=1}^m |C_i - (\bar{X}_i, \bar{U})|^2 - \sum_{i=1}^m |(\bar{X}_i, \bar{U})|^2$$

Since all the quantities on RHS are +ve

For RHS to be minimum

$$C_i = (\bar{X}_i, \bar{U}) \text{ which is the required result.}$$

67) Prove Parseval's eqn.

$$(\bar{U}, \bar{V}) = \sum_{i=1}^n (\bar{X}_i, \bar{U})^* (\bar{X}_i, \bar{V})$$

Now, consider RHS.

$$(\bar{X}_i, \bar{U}) = (\bar{X}_i, \sum_j U_j \bar{X}_j)$$

$$= (\bar{X}_i, U_1 \bar{X}_1) + (\bar{X}_i, U_2 \bar{X}_2) + \dots$$

$$= \sum_j U_j (\bar{X}_i, \bar{X}_j)$$

$$= U_i$$

$$\therefore (\bar{X}_i \bar{U}) = U_i$$

$$\text{similarly } (\bar{X}_i \bar{V}) = V_i$$

$$\therefore \text{RMS} = \sum_i (\bar{X}_i U)^* (\bar{X}_i \bar{V})$$

$$= \sum U_i^* V_i$$

$$= (\bar{U} \bar{V})$$

$$\therefore (\bar{U} \bar{V}) = \sum_{i=1}^n (\bar{X}_i \bar{U})^* (\bar{X}_i \bar{V})$$

(68) If $\bar{U} = LU$ $\bar{V} = LV$

$$|L| \neq 0 \text{ and } V = AU$$

$$\bar{V} = B\bar{U} \text{ then what is } B?$$

Now, we have

$$\bar{V} = LV = LAU$$

$$\text{but } \bar{V} = B\bar{U} \text{ gives } \bar{V} = BLU$$

$$LAU = BLU$$

$$\therefore LA = BL$$

$\therefore B = \cancel{LA} \cancel{A^{-1}} LA L^{-1}$ which is the reqd. relation.

(69) Show that a similarity transformation preserves Algebraic operations.

$$\text{i.e. if } A' = UAU^{-1}, B' = UBU^{-1}$$

$$\text{Then } A'B' = U(AB)U^{-1}$$

$$\& (A'+B') = U(A+B)U^{-1}$$

Now we have:

$$\begin{aligned} \text{A'B'} &= (UAU^{-1})(UBU^{-1}) \\ &= UA(U^{-1}U)BU^{-1} \\ &= U(AB)U^{-1} \end{aligned}$$

$$\begin{aligned} A'+B' &= UAU^{-1} + UBU^{-1} \\ &= U(AU^{-1} + BU^{-1}) \\ &= U(A+B)U^{-1} \end{aligned}$$

Which are the required results.

70) Show that the trace ~~and the~~ of ~~the~~ a matrix is invariant under similarity transformation.

$$\text{Now, Let } A' = UAU^{-1} = BU^{-1} \text{ say}$$

$$\therefore \text{Tr } A' = \text{Tr } BU^{-1}$$

$$\begin{aligned} \therefore \text{Tr } A' &= \text{Tr } (U^{-1}B) \quad \text{since } \text{Tr}(PQ) = \text{Tr}(QP) \\ &= \text{Tr } (U^{-1}UA) \\ &= \text{Tr } A \end{aligned}$$

$$\therefore \text{Tr } A' = \text{Tr } A$$

Thus the trace of a matrix is invariant under similarity transformation.

(71) Show that the determinant of a matrix is invariant under similarity transformations.

$$\text{Let } A' = UAU^{-1}$$

$$\begin{aligned}\therefore \det A' &= \det (UAU^{-1}) \\ &= \det U \det A \det U^{-1} \\ &= \det (UU^{-1}) \det A \\ &= \det I \det A\end{aligned}$$

$$\therefore \det A' = \det A$$

\therefore the determinant of a matrix is invariant under similarity transformations.

(72) Determine A^{-1} for

$$A = \begin{bmatrix} 2 & 3 \\ -3 & 4 \end{bmatrix}$$

Now we have

$$A^{-1} = \frac{A^T}{|A|}$$

$$\text{Now } A^T = \begin{bmatrix} 2 & -3 \\ 3 & 4 \end{bmatrix}$$

$$\text{And } A^T = \text{matrix of cofactors} = \begin{vmatrix} 4 & -3 \\ 3 & 2 \end{vmatrix}$$

$$|A| = 8 + 9 = 17$$

$$\therefore A^{-1} = \begin{vmatrix} 4/17 & -3/17 \\ 3/17 & 2/17 \end{vmatrix}$$

(73) Find B^{-1} for $B = \begin{vmatrix} 1 & 1 & 1 \\ 2 & 4 & -3 \\ 5 & -4 & 1 \end{vmatrix}$

Now we have

$$B^T = \begin{vmatrix} 1 & 2 & 5 \\ 1 & 4 & -4 \\ 1 & -3 & 1 \end{vmatrix}$$

$$\therefore B^+ = \begin{vmatrix} -8 & -5 & -7 \\ -17 & -4 & +5 \\ -28 & 9 & 2 \end{vmatrix}$$

$$|B| = -8 - 15 + 4 - 20 - 12 - 2 = \del{-53} -53$$

$$\therefore B^{-1} = \frac{B^+}{|B|} = \begin{vmatrix} 8/53 & 5/53 & 7/53 \\ 17/53 & 4/53 & -5/53 \\ 28/53 & -9/53 & -2/53 \end{vmatrix}$$

(74) Prove that A^{-1} is unique.

Let $AB = I$ $AC = I$ & $B \neq C$.

Now $B \neq C \Rightarrow AB \neq AC$.

but $AB = I$ & $AC = I$

give $I \neq I$ which is absurd.

This contradiction is due to assumption $B \neq C$.

$$\therefore B = C$$

\therefore Inverse is unique.

75) Show that if

$$C = AB \quad \text{then} \quad C^{-1} = B^{-1}A^{-1}$$

we have

$$(AB)^{-1}(AB) = I$$

$$\therefore (AB)^{-1}(AB)B^{-1} = IB^{-1}$$

$$\therefore (AB)^{-1}A(BB^{-1}) = B^{-1}$$

$$\therefore (AB)^{-1}A = B^{-1}$$

$$\therefore (AB)^{-1} = B^{-1}A^{-1} \quad \text{q.e.d.}$$

76) Show that \sim

$$(\tilde{A})^{-1} = (A^{-1})$$

we have

$$(\tilde{A})^{-1}\tilde{A} = I$$

\therefore multiplying by (A^{-1})

$$(\tilde{A})^{-1}[\tilde{A}(A^{-1})] = (A^{-1})$$

$$\therefore (\tilde{A})^{-1}[A^{-1}A] = (A^{-1})$$

Since $(A^{-1})A = I \in I$

we get

$$(\tilde{A})^{-1} = (A^{-1})$$

(77) Show that $(I+S)(I-S)^{-1}$ is orthogonal if S is a real skew symmetric matrix.

Now, consider

$$\left[(I+S)(I-S)^{-1} \right] \left[(I+S)(I-S)^{-1} \right]$$

$$= (I+S)(I-S)^{-1} (\widetilde{I-S})^{-1} (\widetilde{I+S})$$

$$= (I+S)(I-S)^{-1} (I-\widetilde{S})^{-1} (I+\widetilde{S})$$

$$= (I+S)(I-S)^{-1} (I+S)^{-1} (I-S)$$

Due to skew symmetry.

$$= (I+S) \left[(I+S)(I-S) \right]^{-1} (I-S)$$

$$= I$$

$\therefore (I+S)(I-S)^{-1}$ is idempotent.

(78) Prove that a singular matrix must have at least one eigenvalue zero.

Now, we have, the eigenvalue eqn.

$$\text{Det. } [A - \lambda I] = 0.$$

which is a polynomial eqn. of the n^{th} degree in λ .

$$\lambda^n + (-1)a_1 \lambda^{n-1} + (-1)^2 a_2 \lambda^{n-2} \dots = 0.$$

where $a_n = |A| = 0$ for a singular matrix.

∴ The equ. becomes

$$\lambda [\lambda^{n-1} + (-1)a_1 \lambda^{n-2} + \dots] = 0.$$

which has at least one root $\lambda = 0$.

which is the required result.

(79) If A is a symmetric matrix show that $(\tilde{A}^{-1}) = A^{-1}$

Now we have

$$(\tilde{A}^{-1}) = (\tilde{A})^{-1}$$

But for a symmetric matrix

$$\tilde{A} = A$$

$$\therefore (\tilde{A}^{-1}) = A^{-1} \quad \text{q.e.d.}$$

(80) Find the rank of

$$A = \begin{pmatrix} 1 & 1 & 1 & 1 \\ 2 & 4 & -3 & 9 \\ 3 & 5 & -2 & 11 \end{pmatrix}$$

Now

$$A \xrightarrow{\substack{C_2 - C_1 \\ C_3 - C_1}} \begin{pmatrix} 1 & 0 & 0 & 0 \\ 2 & 2 & -5 & 7 \\ 3 & 2 & -5 & 8 \end{pmatrix} \xrightarrow{R_2 - R_3} \begin{pmatrix} 1 & 0 & 0 & 0 \\ -1 & 0 & 0 & -1 \\ 3 & 2 & -5 & 8 \end{pmatrix}$$

Hence the rank of the matrix is ~~2~~
3. [~~the~~ Largest Nonzero determinant]

81) Solve the characteristic eqn. of the matrix

$$A = \begin{pmatrix} 8 & -12 & 5 \\ 15 & -25 & 11 \\ 24 & -42 & 19 \end{pmatrix}$$

The eigenvalue eqn. is

$$AX = \lambda X$$

& charact. eqn is $\text{Det.}(A - \lambda I) = 0$

$$\begin{vmatrix} 8-\lambda & -12 & 5 \\ 15 & -25-\lambda & 11 \\ 24 & -42 & 19-\lambda \end{vmatrix} = 0.$$

$$= (8-\lambda) \{ (-25-\lambda)(19-\lambda) + 462 \} \\ - 12 \{ 15(19-\lambda) - 264 \} \\ + 5 \{ -630 + 24(25-\lambda) \}$$

$$= \lambda^3 - 2\lambda^2 + \lambda - 2 = 0.$$

$$= (\lambda^2 - 1)(\lambda - 2) = 0.$$

$$\therefore \lambda = +1, -1 \text{ or } +2.$$

Now for $\lambda = 2$ the eqn. for components & eigenvectors become

$$6x_1 - 12x_2 + 5x_3 = 0$$

6-36+30
15-84+66

$$15x_1 - 27x_2 + 11x_3 = 0$$

$$24x_1 - 42x_2 + 17x_3 = 0$$

On solving the eqn. we get

$$x_1 = \frac{1}{\sqrt{46}}, \quad x_2 = \frac{3}{\sqrt{46}}$$

$$x_1 = 1 \quad x_2 = 3 \quad \& \quad x_3 = 6.$$

And normalising, we get the eigenvector

$$\begin{pmatrix} 1/\sqrt{46} \\ 3/\sqrt{46} \\ 6/\sqrt{46} \end{pmatrix}$$

Similarly we can proceed to determine the eigenvectors corresponding to $\lambda = \pm 1$

Thus we can solve the characteristic eqn. of a matrix.

$$\begin{array}{l} 120x_1 - 240x_2 + 100x_3 = 0 \\ 120x_1 - 216x_2 + 88x_3 = 0 \\ 120x_1 - 210x_2 + 85x_3 = 0 \end{array} \quad \left. \begin{array}{l} -24x_2 + 12x_3 = 0 \\ -6x_2 + 3x_3 = 0 \\ x_3 - 2x_2 = 0 \end{array} \right\}$$

X	Y	Z			X	Y	Z
43.88	24.34	27.81	¹ ALA N	⁵ Val N	49.72	24.86	17.47
44.24	25.82	29.77	C ^β		49.00	24.08	15.14
44.24	25.73	28.19	C ^α		49.99	24.16	16.21
45.58	26.34	27.69	C^β		51.25 54.22	25.04	15.89
45.85	27.48	27.88	O		51 54.16	26.26	15.96
46.30	25.47	26.99	² ASP N	⁶ Ala	52.33	24.42	15.45
48.82	25.99	27.37	C ^β		54.85	24.86	15.96
47.56	25.91	28.49	C ^α		53.57	25.12	15.14
47.92	24.86	25.35	C		54.22	24.69	13.81
48.73	23.99	25.61	O		54.13	23.46	13.43
47.29	25.04	24.22	³ THR N	⁷ Val	54.85	25.65	13.18
46.12	23.55	22.83	C ^β		55.11	25.99	10.66
47.47	24.16	23.08	C ^α		55.56	25.30	11.92
48.01	24.95	21.89	C		56.91	25.73	12.49
47.65	26.08	21.70	O		57.18	26.87	12.74
48.82	24.34	21.07	⁴ Ile N	⁸ GLU	57.81	24.69	12.61
50.71	25.65	20.25	C ^β		59.43	23.90	14.25
49.36	24.95	19.88	C ^α		59.16	24.95	13.12
49.72	24.16	18.61	C		60.42	24.77	12.30
50.08	22.94	18.67	O		60.51	23.90	11.42

	X	Y	Z		X	Y	Z
	61.41	25.65	12.55	9Leu ¹³ N P ₁₃ AO	64.32	19.10	15.26
	63.21	26.87	11.10	C ^β	69.14	17.10	14.06
	62.67	25.56	11.79	C ^α	68.69	17.79	15.39
9	63.66	24.95	12.74	C	68.87	16.84	16.59
	64.11	25.56	13.69	O	69.86	16.14	16.71
5	64.02	23.73	12.42	10ASP ¹⁴ N P ₁₄ SN	67.88	16.92	17.41
6	64.38	20.85 21.63	13.75	C ^β	67.16	16.75	19.74
4	65.00	22.94	13.24	C ^α	67.88	16.05	18.61
1	66.44	22.85	12.80	C	67.34	14.65	18.35
3	66.71	22.24	11.79	O	66.17	14.39	18.48
	67.25	23.55	13.50	11THR ¹⁵ N P ₁₅ TR	68.24	13.78	17.91
6	69.32	25.04	13.24	C ^β	69.14	11.51	17.34
	68.69	23.64	13.18	C ^α	67.88	12.39	17.60
9	69.41	22.51	13.88	C	66.89	11.78	18.60
4	70.13	21.72	13.24	O	65.90	11.17	18.29
	69.23	22.42	15.20	12TYR ¹⁶ N P ₁₆ SP	67.25	12.04	19.88
	70.31	21.55	17.47	C ^β	67.07	13.61 11.78	22.33
	69.86	21.37	16.02	C ^α	66.44	11.43	20.94
	69.14	19.98	16.21	C	64.92	11.69	20.94
	68.42	19.98 19.80	17.22	O	64.20	10.99	21.63

X	Y	Z			X	Y	Z	
64.56	12.56	20.06	17 Jle N	21 SEP	68.24	13.26	10.85	60
63.03	14.48	19.87	CB		70.58	12.39	10.72	60
63.12	12.91	19.93	C ^x		69.68	13.52	10.91	61
62.40	12.21	18.73	C		70.40	14.83	10.85	60
61.41	11.51	18.92	O		71.66	14.92	11.10	60
62.94	12.39	17.60	18.61 N	22 JPR	69.68	15.70	10.28	5
					70.40	16.66	08.83	
62.40	11.78	16.34	C ^x		70.31	17.01	09.84	5
62.67	12.65	15.14	C		69.14	17.97	10.03	5
62.13	12.39	14.06	O		68.06	17.53	10.47	5
63.57	13.61	15.26	19 ASP N	23 PRO	69.41	19.19	09.71	5
64.56	15.88	14.44	CB		69.05	21.55	09.59	5
63.93	14.57	14.13	C ^x		68.33	20.24	09.90	5
65.00	13.78	13.37	C		67.07	19.89	09.08	5
65.81	13.08	13.88	O		67.16	19.54	07.95	5
64.92	13.96	12.05	20 PRO N	24 HLS	65.90	20.15	09.78	
65.45	13.70	09.78	CB		64.38	18.40	9.65	5
65.90	13.35	11.16	C ^x		64.65	19.80	9.08	5
67.25	13.61	11.67	C		63.48	20.67	9.52	
67.43	14.13	12.80	O		63.48	21.37	10.53	

62.40	20.67	8.64	²⁵ Ile N	²⁹ Ile	51.79	19.19	16.02
60.78	22.33	7.76	C ^β		49.36	18.41	15.70
61.23	21.37	8.89	C ^α		50.35	19.28	16.46
60.06	20.41	8.89	C		50.35	18.75	17.85
60.06	19.37	8.33	O		50.44	17.53	18.10
58.98	20.85	9.59	²⁶ GLY N	³⁰ Leu	50.17	19.63	18.79
		9.71			49.09	18.14	20.43
57.81	19.98	9.71	C ^α		50.17	19.28	20.25
56.64	20.59	10.60	C		51.43	18.93	20.94
56.82	21.63	11.16	O		51.52	19.10	22.20
55.56	19.80	10.66	²⁷ Ile N	³¹ ser	52.51	18.60	20.18
53.23	19.89	10.53	C ^β		53.68	16.75	20.88
54.40	20.24	11.42	C ^α		53.77	18.32	20.75
54.31	19.63	12.80	C		55.02	18.49	19.93
54.31	18.41	12.93	O		55.02	18.84	18.73
54.04	20.41	13.81	²⁸ ASP N	³² Val	56.19	18.23	20.56
54.94	20.41	16.5 16.27	C ^β		58.62	17.97	20.81
53.94	19.98	15.20	C ^α		57.45	18.41	19.93
52.51	20.24	15.64	C		57.54	17.36	18.73
52.06	21.37	15.64	O		58.08	17.71	17.66

23 AUG 37 THUR

56.91	16.22	18.98	N	57.90	15.70	8.39	6
56.19	15.88 13.96	18.54	C ^B	60.42	15.61	9.27	70
56.82	15.18	17.97	C ^A	59.25	16.22	8.39	6
56.19	15.61	16.65	C	59.79	16.40	7.00	70
55.11	15.18	16.33	O	59.25	15.88	6.05	70
56.91	16.40	15.89	^{34 SER} N	60.87	17.18	6.87	7
57.45	17.62	13.81	C ^B	60.51	18.32	4.73	7
56.37	16.92	14.63	C ^A	61.50	17.36	5.55	7
55.74	15.79	13.81	C	62.85	17.97	5.74	7
56 28	16.40 14.65	13.81	O	63.21	18.67	6.75	7
54.58	16.05	13.18	^{35 LYS} N	63.75	17.79	4.73	-
52.51	15.44	12.36	C ^B	65.99	17.18	4.23	7
53.95	15.00	12.42	C ^A	65.09	18.23	4.79	7
54.49	14.65	11.04	C	65.54	19.54	4.64	7
54.40	13.52	10.53	O	65.45	19.54	2.84	7
55.02	15.70	10.41	^{36 LYS} N	65.90	20.59 24.95	4.79	-
54.76	16.05	07.88	C ^B	65.27	22.68 24.42	4.98	7
55.56	15.53	09.08	C ^A	66.26	21.81	4.23	7
57.00	16.22	09.15	C	67.79	22.16	4.41	-
57.18	17.18	09.90	O	68.33	21.89	5.42	7

(22.77)

1	68.33	22.68	3.34	41 ASP 4562x N	74.27	32.36	8.39
7	70.04	22.77	1.83	CP			
9	69.77	22.94	3.34	C	74.63	33.76	8.07
0	70.31	24.25	3.97	C	74.00	34.28	6.81
5	70.49	25.30	3.28	O	74.27	35.42	6.37
7	70.49	24.25	5.30	42 Met 46675 N	73.10	33.50	6.24
	71.21	24.77	7.44	CP	72.65	32.71	4.04
	70.94	25.38	6.05	C	72.47	33.85	4.98
	72.02	26.26	5.42	C	71.03	34.28	5.23
	73.01	25.73	4.79	O	70.40	33.85	6.24
3	71.84	27.56	5.55	43 Met 47 VAL N	70.49	35.07	4.35
	72.11	28.87	3.72	CP	68.60	36.99	4.23
	72.83	28.52	4.98	C	69.05	35.50	4.48
	73.10	29.48	6.12	C	68.06	34.46	3.97
	72.47	30.53	6.24	O	68.15	33.93	2.90
	74.09	29.13	6.94	44 ASP 4864 N	67.07	34.19	4.86
	75.43	31.40 29.31	9.02	CP	65.99		
	74.45	30.01	8.07	C	65.99	33.23	4.54
	74.90	31.40	7.69	C	64.56	33.76	4.54
	75.70	31.58	6.81	O	64.29	34.89	4.92

63.66	32.89	4.16	49 THR N	53 ITE N	50.53	28.09	4.35
61.77	33.85	2.78	C ^B	C ^P	49.09	28.09	2.59
62.22	33.23	4.10	C ^A	C ^A	49.09	28.18	4.10
61.23	32.10	4.16	C	C	48.10	27.04	4.41
61.14	31.23	3.22	O	O	48.55	25.91	4.54
60.42	32.10	5.17	50A10 N	547A N	46.84	27.39	4.48
59.34	30.79	6.87	C ^B	01	41.99	23.55	9.02
59.34	31.05	5.30	C ^A	02	43.61	26.08	7.06
57.99	31.40	4.86	C	CE2	42.62	25.38	7.76
57.54	32.54	4.86	O	C2	42.98	24.16	8.39
57.18	30.36	4.54	51MS N	CE1	44.24	23.73	8.39
55.65	30.44	2.52	C ^B	01	45.22	24.42	7.69
55.83	30.53	4.04	C ^A	CG	44.96	25.65	7.06
54.94	29.40	4.60	C	EP ^B	46.03	26.34	6.31 6.31
55.38	28.26	4.86	O	C ^A	45.76	26.43	4.79
53.68	29.75	4.73	ite N	C	44.33	26.95	4.79
52.87	28.87	6.75	C ^B	O	44.06	28.09	4.67
52.89	28.79	5.23	C ^A	55PSN N	43.43	25.99	4.86
51.16	29.05	5.05	C	C ^B	41.72	26.95	3.47
50.62	30.00	5.49	O	C ^A	41.99	26.34	4.86

					C	43.70	20.76	5.68
5	41.09	25.12	5.05		O	43.88	19.71	6.31
	41.54	23.90	4.79		O	⁶⁰ ARG N 44.60	21.37	4.92
	39.92	25.38	5.49		⁵⁶ SER N C ^β	46.12	20.15	3.41
	37.85	25.99	7.06		OG C ^α	45.94	20.76	4.79
	37.94	25.38	5.74		C ^β C	47.11	21.72	5.11
	38.93	24.25	5.68		C ^α O	47.47	22.59	4.35
	38.48	23.38	4.54		C	⁶¹ Leu N 47.65	21.55	6.31
	38.48	22.16	4.67		O C ^β	49.18	22.24	8.26
	38.12	23.99	3.41		⁵⁷ VAL N C ^α	48.82	22.33	6.75
	37.58	23.73	0.82		C ^β C	50.08	22.24	5.93
	37.76	23.29	2.21		C ^α O	50.80	21.28	5.99
	38.75	22.07	2.27		C	⁶² SER N 50.35	23.29	5.11
	38.30	20.94	2.52		O C ^β	50.98	23.64	2.90
631	40.01	22.42	2.02		⁵⁸ ASP N C ^α	51.52	23.29	4.23
	42.26	21.98	1.39		C ^β C	52.60	24.34	4.35
	41.00	21.37	2.08		C ^α O	52.24	25.56	4.68
	41.63	20.94	3.34		C	⁶³ ALA N 53.86	23.99	4.23
	42.08	19.71	3.47		O C ^β	55.74	24.42	5.55
	41.72	21.81	4.35		⁵⁹ LYS N C ^α	54.94	24.95	4.35
	41.27	20.50	6.24		C ^β C	56.10	24.95	3.34
	42.35	21.46	5.61		C ^α O	56.37 627	23.90 224.274	2.71 4.43

0.08991

0.08723

0.06307

X

Y

Z

630	56.64	300	⁶⁴ VAL N	26.17	50	3.15
635	57.09	299 307	CB	26.78	15	0.95
643	57.81	302	CK	26.34	35	2.21
655	58.89	312	C	27.22	44	2.78
653	58.71	326	O	28.44	46	2.90
667	59.97	305	⁶⁵ VAL N	26.61	49	3.09
685	61.59	307	CB	26.78	78	4.92
680	61.14	314	CK	27.39	57	3.59
691	62.13	315	C	27.48	39	2.46
699	62.85	304	O	26.52	33	2.08
693	62.31	329	⁶⁶ SER N	28.70	31	1.96
694	42.40	340	CB	29.66	-2	-0.13
703	63.21	332	CK	28.96	13	0.82
717	64.47	340	C	29.66	18	1.14
719	64.65	348	O	30.36	35	2.21
728	65.45	339	⁶⁷ TR N	29.57	3	0.19
755	67.88	337	CB	29.40	12	0.76
742	66.71	347	CK	30.27	6	0.38
746	67.07	353	C	30.79	-16	-1.01
742	66.71	345	O	30.09	-31	-1.96

X

Y

Z

68 PRO

752	67.61	366	N	31.93	-17	-1.07
760	68.33	389	CP	33.93	-33	-2.08
756	67.97	373	C ^A	32.54	-38	-2.40
768	69.05	364	C	31.75	-50	-3.15
780	70.13	361	O	31.49	-42	-2.65
764	68.69	360	69 ASP N	31.40	-70	-4.41
791	71.12	357	CP	31.14	-82	-5.17
775	69.68	352	C ^A	30.70	-84	-5.30
773	69.50	335	C	29.22	-77	-4.86
774	69.59	325	O	28.35	-91	-5.74
770	69.23	333	70 ALA N	29.05	-57	-3.59
771	69.32	317	CP	27.65	-25	-1.58
768	69.05	317	C ^A	27.65	-49	-3.09
753	67.70	311	C	27.13	-54	-3.41
742	66.71	320	O	27.91	-58	-3.66
751	67.52	296	71 ASP N	25.82	-54	-3.41
741	66.62	274	CP	23.90	-72	-4.54
737	66.26	288	C ^A	25.12	-59	-3.72
726	65.27	286	C	24.95	-41	-2.59
730	65.63	285	O	24.86	-22	-1.39

	X	Y	Z		X	Y	Z	
72ALA	6712	286	-46	76SER	599	218	65	80
N	64.02	24.95	-2.90	N	53.86	19.02	4.10	
CB	685 61.59	287 25.04	-41 -2.59		576 51.79	217 18.93	46 2.90	
CA	700 62.94	285 24.86	-30 -1.89		583 52.42	220 19.19	67 4.23	
C	697 62.67	270 23.55	-17 -1.07		575 51.70	207 18.06	80 5.05	
O	698 62.76	257 22.42	-25 -1.58		577 51.88	194 16.92	77 4.86	
73THR	693	273	2	77TR	566	213	95	81
N	62.31	23.81	0.13		50.89	18.58	5.99	
CB	702 63.12	262 22.85	34 2.14		566 50.89	201 17.53	131 8.26	
CA	690 62.04	260 22.68	17 1.07		558 50.17	202 17.62	109 6.87	
C	674 60.60	262 22.85	25 1.58		541 48.64	205 17.88	110 6.94	
O	670 60.24	274 23.90	35 2.21		536 48.19	218 19.02	110 6.94	
74SER	665	251	21	78ASP	533	192	110	83
N	59.79	21.89	1.32		47.92	16.75	6.94	
CB	641 57.63	253 22.07	9 0.57		507 45.58	180 15.70	101 6.37	
CA	649 58.35	252 21.98	28 1.77		517 46.48	193 16.84	110 6.94	
C	643 57.81	237 20.67	40 2.52		511 45.94	193 16.84	133 8.39	
O	650 58.44	225 19.63	38 2.40		513 46.12	182 15.88	145 9.15	
75Val	631	239	51	79Val	504	206	138	83
N	56.73	20.85	3.22		45.31	17.97	8.70	
CB	631 56.73	225 19.63	85 5.36		511 45.94	215 18.75	171 10.78	
CA	625 56.19	227 19.80	63 3.97		498 44.78	200 208 18.14	160 10.09	
C	608 54.67	230 20.06	65 4.10		484 43.52	218 19.02	161 10.15	
O	603 54.22	243 21.20	66 4.16		482 43.34	228 19.89	148 9.33	

80 ASP	478	216	178	84 Val	457	244	261
N	42.80	18.84	11.23		41.09	21.28	16.46
CB	450	214	189		485	245	266
	40.46	18.67	11.92		43.61	21.37	16.78
C ²	462	225	181		470	247	276
	41.54	19.63	11.42		42.26	21.55	17.41
C	464	237	199		472	263	286
	41.72	20.67	12.55		42.44	22.94	18.04
C	462	233	218		473	264	306
	41.54	20.32	13.75		42.53	23.03	19.30
81 Lew	469	250	193	85 ASP Lew	471	275	273
	42.17	21.81	12.17		42.35	23.99	17.22
	480	274	194		477	300	261
	43.16	23.90	12.24		42.89	22 2617	16.46
	472	262	208		473	291	281
	42.44	22.85	13.12		42.53	25.38	17.72
	457	266	218		459	297	291
	41.09	23.20	13.75		41.27	25.91	18.35
	456	270	237		446	293	288
	41.00	23.55	14.95		40.10	25.56	18.04
	82 ASN	445	264	205	86 PRO	461	309
40.01		23.03	12.93		41.45	26.95	19.24
417		261	199		456	323	335
37.49		22.77	12.55		41.00	28.18	21.13
430		267	213		446	316	316
38.66		23.29	13.43		40.10	27.56	19.93
449		257	234		442	325	298
40.37		22.42	14.76		39.74	28.35	18.79
426		263	250		449	331	284
38.30		22.94	15.77		40.37	28.87	17.91
83 ASP	424	243	232	87 Lew	427	337	299
	38.12	21.20	14.63		38.39	29.40	19.86
	434	216	245		401	335	286
	39.02	18.84	15.45		36.05	29.22	18.04
	434	233	251		419	335	283
	39.02	20.32	15.83		37.67	29.22	17.85
	445	236	268		426	351	278
	40.01	20.59	16.90		38.30	30.62	17.53
	444	232	287		426	356	261
39.92	20.24	18.10		38.30	31.05	16.46	

88 TRP	433	357	295	9267	577	395	266	96
N	38.93	31.14	18.61	N	51.88	34.46	16.78	N
CB	434 39.02	383 33.41	308 19.43	CB				CB
CA	441 39.65	372 32.45	293 18.47	CA	592 53.23	401 34.98	273 17.22	CA
C	457 41.09	369 32.19	299 18.86	C	606 54.49	394 34.37	264 16.65	C
O	460 41.36	364 31.75	317 19.99	O	605 54.40	385 33.58	249 15.70	O
89 VAL	467	372	284	9356	618	398	274	97
N	41.99	32.45	17.91	N	55.56	34.72	17.28	N
CB	488 43.88	359 31.32	271 17.09	CB	640 57.54	403 35.15	251 15.83	CB
CA	483 43.43	370 32.28	289 18.23	CA	633 56.91	392 34.19	266 16.78	CA
C	493 44.33	384 33.50	289 18.23	C	642 57.72	385 33.58	284 17.91	C
O	488 43.88	397 34.63	286 18.04	O	644 57.90	392 34.19	301 18.98	O
90 ARG	507	381	292	9456	649	372	280	98
N	45.58	33.23	18.42	N	58.35	32.45	17.66	N
CB	522 46.93	392 34.19	316 19.93	CB	650 58.44	351 30.62	305 19.24	CB
CA	518 46.57	394 34.37	293 18.48	CA	658 59.16	364 31.75	295 18.61	CA
C	532 47.83	389 33.93	279 17.60	C	673 60.51	359 31.32	285 17.97	C
O	535 48.10	375 32.71	277 17.47	O	674 60.60	356 31.05	266 16.78	O
91 VAL	539	400	269	95 ALA	685	359	298	99
N	48.46	34.89	16.97	N	61.59	31.32	18.79	N
CB	546 49.09	403 35.15	234 14.76	CB	712 64.02	367 32.01	289 18.23	CB
CA	551 49.54	398 34.72	256 16.34	CA	699 62.85	354 30.88	290 18.29	CA
C	566 50.89	405 35.33	263 16.59	C	707 63.57	348 30.36	310 19.55	C
O	567 50.98	419 36.55	266 16.78	O	702 63.12	353 30.79	328 20.69	O

96 SER	718	339	307	1007R	816	287	350
N	64.56	29.57	19.36		73.37	25.04	22.07
CB	718	317	331		818	281	318
	64.56	27.65	20.88		73.55	24.51	20.06
CA	725	332	326		822	294	335
	65.18	28.96	20.56		73.91	25.65	21.13
C	742	329	327		818	310	330
	66.71	28.70	20.62		73.55	27.04	20.81
O	750	327	311		806	316	336
	67.43	28.52	19.61		72.47	27.56	21.19
97 THR	748	329	347	101 LYS	828	318	320
N	67.25	28.70	21.89		74.45	27.74	20.18
CB	771	342	351		843	339	317
	69.32	29.83	22.14		75.79	29.57	19.99
CA	763	326	351		827	334	314
	68.60	28.44	22.14		74.36	29.13	19.80
C	765	317	372		820	336	292
	68.78	27.65	23.46		73.73	29.31	18.42
O	755	317	385		823	326	278
	67.88	27.65	24.28		74.00	28.44	17.53
98 GLY	777	309	374	102 GLU	813	349	288
N	69.86	26.95	23.59		73.10	30.44	18.16
CB	7				795	339	263
					71.48	29.57	16.59
CA	780	300	393		806	352	267
	70.13	26.17	24.79		72.47	30.70	16.84
C	796	297	400		798	367	270
	71.57	25.91	25.23		71.75	32.01	17.03
O	802	303	415		794	372	287
	72.11	26.43	26.17		71.39	32.45	18.10
99 LEU	803	286	388	103 THR	796	375	252
N	72.20	24.95	24.47		71.57	32.71	15.88 89
CB	815	266	381		797	402	241
	73.28	23.20	24.03		71.66	35.07	15.20
CA	818	281	393		788	389	251
	73.55	24.51	24.79		70.85	33.93	15.83
C	825	288	373		772	386	243
	74.18	25.12	23.53		69.41	33.67	15.33
O	837	295	373		770	376	230
	75.25	25.73	23.53		69.23	32.90	14.51

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104				SEA				112
	762	395	251	108	684	467	126	THR
N	68.51	34.46	15.86	N	61.50	40.74	7.95	N
CB	736	382	256	CB	670	470	97	CB
	66.17	33.32	16.15		60.24	41.00	6.12	
CA	746	394	244	CA	669	471	120	CA
	67.07	34.37	15.39		60.15	41.09	7.57	
C	740	410	241	C	658	459	129	C
	66.53	35.76	15.20		59.16	40.04	8.14	
O	731	415	254	O	662	445	183	O
	65.72	36.20	16.02		59.52	38.82	8.39	
THR	744	417	224	TRPP9	644	464	182	SEA
105 N	66.89	36.37	14.13	N	57.90	40.47	8.33	N
CB	754	439	217	CB	632	451	164	OC
	67.79	38.29	13.69		56.82	39.34	10.34	CB
CA	739	432	219	CA	633	453	136	CA
	66.44	37.68	13.81		56.91	39.52	8.83	C
C	728	432	201	C	618	458	181	C
	65.45	37.68	12.68		55.56	39.95	8.26	
O	729	424	185	O	613	471	182	C
	65.54	36.99	11.67		55.11	41.09	8.33	
106	716	441	263	SEA 110	610	447	122	C
11E	64.38	38.47	12.80	N	54.85	38.99	7.69	C
N	690	439	200	CB	597	451	88	114
CB	62.04	38.29	12.61		53.68	39.34	5.55	N
CA	704	432	187	CA	596	449	112	C
	63.30	37.68	11.79		53.59	39.17	7.06	C
C	706	458	176	C	583	438	117	C
	63.48	39.95	11.10		52.42	38.21	7.38	
107	708	470	186	O	586	424	116	C
11E	63.66	41.00	11.73	O 111	52.69	36.99	7.32	C
N	706	457	155	N	570	444	122	C
	63.48	39.86	9.78		51.25	38.73	7.69	11E
CB	720	467	130	CA	555	433	151	N
	64.74	40.74	8.20		49.90	37.77	9.52	C
CA	708	471	142	CB	557	434	127	C
	63.66	41.09	8.96		50.08	37.86	8.01	C
C	692	477	137	C	543	438	117	C
	62.22	41.61	8.64		48.82	38.21	7.38	
O	688	489	143	O	537	451	120	C
	61.86	42.66	9.02		48.28	39.34	7.57	
107	Leu							

0123

112	537	427	106	116	390	385	81
THR							
N	48.28	37.25	6.69	N	35.06	33.58	5.11
CB	526	436	21	CB	384	375	49
	47.29	38.03	4.48		34.53	32.71	3.09
CA	522	429	95	CA	377	385	67
	46.93	37.42	5.99		33.90	33.58	4.23
C	511	417	102	C	362	380	76
	45.94	36.37	6.43		32.55	33.15	4.79
O	516	403	104	O	360	366	82
	46.39	35.15	6.56		32.37	31.93	5.17
SER112	498	421	106	SER117	351	390	76
N	44.78	36.72	6.69	N	31.56	34.02	4.79
OG	482	414	151	CB	334	400	98
	43.34	36.11	9.52		30.03	34.89	6.18
CB	490	406	131	CA	336	386	84
	44.06	35.42	8.58		30.21	33.67	5.30
CA	486	411	113	C	324	382	69
	43.70	35.85	7.13		29.13	33.32	4.35
C	470	415	112	O	326	381	50
	42.26	36.20	7.06		29.31	33.23	3.15
O	465	427	121	ASN118	310	381	78
	41.81	37.25	7.63	N	27.87	33.23	4.92
114	462	406	100	CB	283	371	78
N	41.54	35.42	6.31		25.44	32.36	4.92
CB	445	415	74	CA	297	377	66
	40.01	36.20	4.68		26.70	32.89	4.16
CA	446	410	97	C	296	391	56
	40.10	35.76	6.12		26.07	34.11	3.53
C	433	398	100	O	285	391	37
	38.93	34.72	6.31		25.62	34.11	2.33
O	436	384	99	SER119	289	403	68
	39.20	33.50	6.24	N	25.98	35.15	4.29
115	420	404	104	CB	292	429	71
N	37.76	35.24	6.56		26.25	37.42	4.48
CB	404	398	131	CA	282	417	60
	36.32	34.72	8.26		25.35	36.37	3.78
CA	407	394	107	C	283	421	37
	36.59	34.37	6.75		25.44	36.72	2.33
C	393	396	94	O	271	421	26
	35.33	34.54	5.93		24.37	36.72	1.64
O	385	407	96				
	34.62	36.50	6.05				

THA120 246 423 29

ASP124

N	26.61	36.90	1.83
CB	294	442	1
	26.43	38.56	0.06
CA	299	426	6
	26.88	37.16	0.38
C	315	422	2
	28.32	36.81	0.13
O	318	408	-3
	28.59	35.59	-0.19

N	384	441	106
CB	34.53	38.47	6.69
	390	448	142
CA	35.06	39.08	8.96
	396	446	120
C	35.60	38.90	7.57
	413	444	116
O	37.13	38.73	7.32
	417	432	107
	37.49	37.68	6.75

HSA121

N	325	433	5
CB	29.22	37.77	0.32
	348	432	-20
CA	31.29	37.68	-1.26
	341	430	1
C	30.66	37.51	0.06
	351	442	10
O	31.56	38.56	0.63
	347	455	17
	31.20	39.69	1.07

ALP125

N	422	454	124
CB	37.94	39.60	7.82
	440	457	98
CA	39.56	39.86	6.18
	438	453	122
C	39.38	39.52	7.69
	450	464	129
O	40.46	40.47	8.14
	448	478	132
	40.28	41.70	8.33

GLN122

N	365	438	11
CB	32.82	38.21	0.69
	380	464	13
CA	34.17	40.47	0.82
	377	448	20
C	33.90	39.08	1.26
	374	452	43
O	33.63	39.43	2.71
	375	465	49
	33.72	40.56	3.09

LOU126

N	465	457	132
CB	41.63	39.86	8.33
	477	462	162
CA	42.89	40.30	10.22
	475	466	138
C	42.80	40.65	8.70
	493	465	131
O	44.33	40.56	8.26
	498	453	127
	44.78	39.52	8.01

THA123

N	369	441	55
CB	33.18	38.47	3.47
	354	428	83
CA	32.28	37.23	5.23
	366	443	78
C	32.91	38.64	4.92
	378	450	91
O	33.99	39.25	5.74
	383	463	88
	34.44	40.39	5.55

HSA127

N	500	478	129
CB	44.96	41.70	8.14
	516	483	99
CA	46.39	42.13	6.24
	515	479	122
C	46.30	41.78	7.69
	526	488	136
O	47.29	42.57	8.58
	523	500	145
	47.02	47.5	9.15

43.62

128 Phe

N	540 48.55	482 42.04	138 8.70
β	550 49.45	488 42.57	174 10.97
γ	552 49.63	489 42.66	150 9.46
C	566 50.89	489 42.66	138 8.70
O	572 51.43	476 41.52	133 8.39

Met 129

N	572 51.43	502 43.79	134 8.45
β	585 52.60	510 44.49	100 6.31
γ	586 52.69	503 43.88	123 7.76
C	601 54.04	509 44.40	134 8.45
O	601 54.04	521 45.45	143 9.02

Phe 130

N	612 55.02	500 43.42	132 8.33
β	630 56.64	495 43.18	162 10.22
γ	627 56.37	504 43.96	142 8.96
C	641 57.63	503 43.88	129 8.14
O	645 57.99	492 42.92	119 7.51

Asn 131

N	650 58.44	515 44.92	131 8.26
β	659 59.25	527 45.97	101 6.37
γ	664 59.70	516 45.01	120 7.57
C	676 60.78	523 45.62	135 8.51
O	689 61.95	524 45.71	129 8.14

GLN

β	671 60.33	528 46.06	153 9.65
γ	687 61.77	550 47.98	163 10.28
δ	681 61.23	535 46.67	169 10.66
E	672 60.42	538 46.93	189 11.92
F	661 59.43	546 47.63	189 11.92

Phe 133

N	678 60.96	532 46.41	207 13.06
β	674 60.60	519 45.27	239 15.07
γ	671 60.33	534 46.58	227 14.32
C	677 60.87	548 47.80	238 15.01
O	689 61.95	554 48.33	232 14.63

SER 134

N	669 60.15	554 48.33	254 16.02
β	661 59.43	579 50.51	263 16.59
γ	674 60.60	567 49.64	265 16.71
C	678 60.96	566 49.37	289 18.23
O	677 60.87	553 48.24	298 18.79

Lys 135

N	683 61.41	578 50.42	298 18.79
β	696 62.58	592 51.64	329 20.75
γ	687 61.77	578 50.42	320 20.18
C	672 60.42	598 50.42	329 20.75
O	669 60.15	573 49.98	347 21.89

ASP 136			
N	661	584	316
	59.43	50.94	19.93
CB	640	600	313
	57.54	52.34	19.74
C ^x	646	585	323
	58.08	51.03	20.37
C	639	569	319
	57.45	49.63	20.12
O	637	560	334
	57.27	48.85	21.07

GLN 137			
N	634	567	300
	57.00	49.46	18.92
CB	635	538	288
	57.02	46.93	18.16
C ^x	627	552	294
	56.37	48.15	18.54
C	616	550	312
	55.38	47.98	19.68
O	619	541	327
	55.65	47.19	20.62

LSP 138			
N	603	558	310
	54.22	48.67	19.55
CB	589	572	335
	52.78	49.90	21.13
C ^x	592	556	326
	53.23	48.50	20.56
C	578	546	322
	51.97	47.63	20.31
O	570	543	336
	51.25	47.37	21.19

ASP 139			
N	577	541	302
	51.88	47.19	19.05
CB	558	539	276
	50.17	47.02	17.41
C ^x	565	531	296
	50.80	46.32	18.67
C	572	515	294
	51.43	44.92	18.54
O	568	506	280
	51.07	44.14	17.66

Lew 40			
N	582	512	308
	52.33	44.66	19.43
CB	605	501	299
	54.40	43.70	18.86
C ^x	590	497	308
	53.05	43.35	19.43
C	591	491	331
	53.14	42.83	20.88
O	593	500	345
	53.32	43.62	21.76

Lew 41			
N	590	476	333
	53.05	41.52	21.00
CB	579	458	362
	52.06	39.95	22.83
C ^x	592	469	354
	53.23	40.91	22.33
C	606	459	355
	54.49	40.04	22.39
O	606	446	347
	54.49	38.90	21.89

Lew 42			
N	617	466	364
	55.47	40.65	22.96
CB	643	471	366
	57.81	41.09	23.08
C ^x	632	458	365
	56.82	39.95	23.02
C	633	449	386
	56.91	39.17	24.35
O	627	454	403
	56.37	39.60	25.42

GLN 143			
N	640	435	385
	57.54	37.95	24.28
CB	632	411	404
	56.82	35.85	25.48
C ^x	641	426	404
	57.63	37.16	25.48
C	658	424	408
	59.16	36.99	25.73
O	667	425	394
	59.97	37.07	24.85

GLY 124

	662	422	428
N	59.52	36.81	26.99
M	677	420	435
	60.87	36.64	27.44
C	690	430	429
	62.04	37.51	27.06
O	692	443	437
	62.22	38.64	27.56

ASP 145

	700	424	415
N	62.94	36.99	26.17
CB	728	425	413
	65.45	37.07	26.05
M	713	433	408
	64.11	37.77	25.73
C	713	440	386
	64.11	38.38	24.35
O	724	444	377
	65.09	38.73	23.78

ALFA 145

	700	440	377
N	62.94	38.38	23.78
CB	681	446	352
	61.23	38.90	22.20
M	698	446	355
	62.76	38.90	22.39
C	702	463	357
	63.12	40.39	22.52
O	701	470	374
	63.03	41.00	23.59

147 THR

	708	469	340
N	63.66	40.91	21.44
CB	729	489	343
	65.54	42.66	21.63
M	712	486	339
	64.02	42.39	21.38
C	707	493	319
	63.57	43.00	20.12
O	709	486	301
	63.75	42.39	18.98

148 THR

	700	506	320
N	62.94	44.14	20.18
CB	678	519	300
	60.96	45.27	18.92
M	694	514	302
	62.40	44.84	19.05
C	703	529	300
	63.21	46.14	18.92
O	706	536	316
	63.48	46.76	19.93

149 GLY

	701	533	281
N	63.57	46.49	17.72
M	716	574	277
	64.38	50.07	17.47
C	733	545	279
	65.90	47.54	17.60
O	741	556	274
	66.62	48.50	17.28

150 THR

	738	532	287
N	66.35	46.41	18.10
CB	757	512	287
	68.06	44.66	18.10
M	754	529	290
	67.79	46.14	18.29
C	762	537	272
	68.51	46.84	17.16
O	772	547	276
	69.41	47.71	17.41

151 ASP

	759	532	252
N	68.24	46.41	15.89
CB	777	527	223
	69.86	45.97	14.06
M	767	539	234
	68.96	47.02	14.76
C	754	542	219
	67.79	47.28	13.81
O	756	543	199
	67.97	47.37	12.55

152GL1

	741	545	228
N	66.62	47.54	14.38
	728	548	215
C	65.45	47.80	13.56
	721	533	208
C	64.83	46.49	13.12
	715	532	190
O	64.29	46.41	11.98

153ASN	722	522	221
N	64.92	45.53	13.94
	730	496	211
CP	65.63	43.27	13.31
	717	506	216
C	64.47	44.14	13.62
	709	499	235
C	63.75	43.53	14.82
	711	504	253
O	63.93	43.96	15.96

Leu 64	701	486	231
N	63.03	42.39	14.57
	679	470	245
CP	61.05	41.00	15.45
	694	478	248
C	62.40	41.70	15.64
	706	466	251
C	63.48	40.65	15.83
	710	457	236
O	63.84	39.86	14.88

155GLU	712	465	270
N	64.02	40.56	17.03
	736	464	287
CP	66.17	40.47	18.10
	724	454	275
C	65.09	39.60	17.34
	717	444	292
C	64.47	38.73	18.42
	717	448	311
O	64.47	39.08	19.61

151Leu

	712	430	286
N	64.02	37.51	18.04
	697	407	289
CP	62.67	35.50	18.23
	706	420	301
C	63.48	36.64	18.98
	716	415	319
C	64.38	36.20	20.12
	712	414	337
O	64.02	36.11	21.25

157THR	730	412	312
N	65.63	35.94	19.68
	752	395	318
CP	67.61	34.46	20.06
	741	407	328
C	66.62	35.50	20.69
	753	418	334
C	67.70	36.46	21.19
	756	430	326
O	67.97	37.51	20.56

158ARG	759	415	355
N	68.24	36.20	22.39
	781	426	383
CP	70.22	37.16	24.16
	770	425	364
C	69.23	37.07	22.96
	785	429	354
C	70.58	37.42	22.33
	795	419	352
O	71.48	36.55	22.20

159VAL	787	443	348
N	70.76	38.64	21.95
	795	453	316
CP	71.48	39.52	19.93
	800	448	338
C	71.93	39.08	21.32
	810	459	350
C	72.83	40.04	22.07
	805	468	364
O	72.38	40.82	22.96

160SER	825	459	345	164SER	862	437	297
N	74.18	40.04	21.76	N	77.50	38.12	18.73
B	850	461	356	B	872	431	329
	76.42	40.21	22.45		78.40	37.60	20.75
	835	469	356		862	424	312
C	75.07	40.91	22.45	C	77.50	36.99	19.68
	838	484	342		847	418	320
C	75.34	42.22	21.57	C	76.15	36.46	20.18
	831	486	326		841	423	336
O	74.72	42.39	20.56	O	75.61	36.90	21.19
161SER	848	493	350	165PRO	841	407	307
N	76.24	43.00	22.07	N	75.61	35.50	19.36
B	857	520	353	B	824	390	295
	77.05	45.36	22.26		74.09	34.02	18.61
	852	507	339		827	401	313
C	76.60	44.23	21.38	C	74.36	34.98	19.74
	862	506	319		829	394	335
C	77.50	44.14	20.12	C	74.54	34.37	21.13
	864	517	307		840	385	339
O	77.68	45.10	19.36	O	75.52	33.58	21.38
162PSN	868	493	316	166GLW	818	397	349
N	78.04	43.00	19.93	N	73.55	34.63	22.01
B	893	484	308	B	809	401	385
	80.29	42.22	19.43		72.74	34.98	24.28
	878	490	298		819	391	370
C	78.94	42.74	18.79	C	73.64	34.11	23.34
	871	478	283		813	375	370
C	78.31	41.70	17.85	C	73.10	32.71	23.34
	876	475	265		806	370	354
O	78.76	41.43	16.71	O	72.47	32.28	22.33
163GLY	859	471	291	167GLY	815	367	387
N	77.23	41.09	18.35	N	73.28	32.01	24.41
C	857	459	279	C	810	351	389
	76.51	40.04	17.60		72.83	30.62	24.53
	850	446	296		799	349	408
C	76.42	38.90	18.67	C	71.84	30.44	25.73
	840	446	309		796	360	420
O	75.52	38.90	19.49	O	71.57	31.40	26.49

168 SER	793	336	410
N	71-30	29-31	25-86
CB	789 70-94	329 28-70	448 28-26
CA	782 70-31	332 28-96	427 26-93
C	769 69-14	344 30-01	427 26-93
O	764 68-69	349 30-44	444 28-00

169 SER	765	349	408
N	68-78	30-44	25-73
CB	780 68-33	337 375	403 396
CA	753 67-70	356 361	406 406
C	738 66-35	357 357	406 397
O	736 66-17	346 30-18	386 24-35

170 VAL	727	367	402
N	65-36	32-01	25-35
CB	706 63-48	352 30-70	407 25-67
CA	712 64-02	365 31-84	394 24-85
C	700 62-94	378 32-97	397 25-04
O	697 62-67	383 33-41	415 26-17

171 GLY	693	382	379
N	62-31	33-32	23-90
CA	682 61-32	394 34-37	380 23-97
C	673 60-51	393 34-28	359 22-64
O	677 60-87	386 33-67	344 21-70

172 PRG	661	402	359
N	59-43	35-07	22-64
CB	639 57-45	391 34-11	343 21-63
CA	651 58-53	403 35-15	340 21-44
C	641 57-63	417 36-37	339 21-38
O	641 57-63	426 37-16	354 22-33

173 ALP	633	418	322
N	56-91	36-46	20-31
CB	632 56-82	445 38-82	309 19-49
CA	623 56-01	431 37-60	319 20-12
C	610 54-85	429 37-42	304 19-17
O	611 54-94	421 36-72	288 18-16

174 LEU	597	435	311
N	53-68	37-95	19-61
CB	574 51-61	421 36-72	310 19-55
CA	584 52-51	433 37-77	298 18-79
C	575 51-70	448 39-08	294 18-54
O	575 51-70	458 39-95	307 19-36

175 PHE	568	448	276
N	51-07	39-08	17-41
CB	550 49-45	461 40-21	249 15-70
CA	559 50-26	462 40-30	270 17-03
C	547 49-18	464 40-47	286 18-04
O	541 48-64	453 39-52	295 18-61

	458	400	239
	41.18	34.89	15.07
O	455	393	255
	40.91	34.28	16.08

176			
TRK	544	479	291
N	48.91	41.78	18.35
CB	534	500	311
	48.01	43.62	19.61
CA	532	488	307
	47.83	42.57	19.36
	517	475	303
C	46.48	41.43	19.11
	512	466	315
O	46.03	40.65	19.87

180 HHS	450	399	221
N	40.46	34.80	13.94
CB	421	396	215
	37.85	34.54	13.56
CA	437	390	220
	39.29	34.02	13.88
C	437	376	206
	39.29	32.80	12.99
	435	377	187
O	39.11	32.89	11.79

181 APL	511	480	285
N	45.94	41.87	17.97
CB	487	484	264
	43.79	42.22	16.65
CA	496	474	279
	44.60	41.35	17.60
	495	457	277
C	44.51	39.86	17.47
	503	449	265
O	45.22	39.17	16.71

182 TRP	440	363	216
N	39.56	31.66	13.62
CB	452	338	217
	40.64	29.48	13.69
CA	440	349	205
	39.56	30.44	12.93
	427	343	192
C	38.39	29.92	12.11
	427	342	172
O	38.39	29.83	10.85

183 APL	484	450	287
N	43.52	39.25	18.10
CB	419 469	431	302
	42.17	37.60	19.05
CA	481	433	286
	43.25	37.77	18.04
	478	430	263
C	42.98	37.51	16.59
	475	440	250
O	42.80	38.38	15.77

184 TRP	415	340	203
N	37.31	29.66	12.80
CB	399	320	207
	35.87	27.91	13.06
CA	401	334	193
	36.05	29.13	12.17
	388	342	203
C	34.89	29.83	12.80
	389	348	221
O	34.97	30.36	13.94

189 VAL	476	415	259
N	42.80	36.20	16.34
CG2	499	410	277
	44.87	35.76	17.47
GG1	483	391	209
	43.43	34.11	13.18
CB	486	400	229
	43.70	34.89	14.44
CA	472	410	238
	42.44	35.76	15.01

183 GLW	375	341	193
N	33.72	29.75	12.17
CB	363	364	194
	32.64	31.75	12.24
CA	361	347	201
	32.46	30.27	12.68
	346	341	195
C	31.11	29.75	12.30
	344	331	181
O	30.93	28.87	11.42

184 SER

N	335 30.12	347 30.27	205 12.93
CB	306 27.51	351 30.62	209 13.18
CA	319 28.68	343 29.92	201 12.68
C	315 28.32	340 29.66	177 11.16
O	312 28.05	327 28.52	171 10.78

185 SER

N	316 28.41	353 30.79	165 10.41
CB	302 27.15	366 31.93	139 8.77
CA	312 28.05	352 30.70	143 9.02
C	325 29.22	352 30.70	127 8.01
O	323 29.04	356 31.05	108 6.81

186 SER

N	338 30.39	348 30.36	135 8.51
CB	365 32.82	347 30.27	136 8.58
CA	351 31.56	347 30.27	122 7.69
C	353 31.74	331 28.87	112 7.06
O	352 31.65	320 27.91	124 7.82

187 SER

N	354 31.83	331 28.87	92 5.80
CB	340 30.57	318 27.74	70 4.41
CA	356 32.01	316 27.56	80 5.05
C	370 33.27	316 27.56	67 4.23
O	374 33.63	304 26.52	58 3.66

188 VAL

N	377 33.90	329 28.70	66 4.16
CB	384 34.53	337 29.40	34 2.14
CA	391 35.15	331 28.87	54 3.41
C	402 36.14	341 29.75	65 4.10
O	401 36.05	356 31.05	63 3.97

189 SER

N	412 37.04	335 29.22	77 4.86
OG	432 38.84	351 30.62	124 7.82
CB	424 38.12	340 29.66	112 7.06
CA	424 38.12	344 30.01	88 5.55
C	440 39.56	342 29.83	81 5.11
O	444 39.92	331 28.87	71 4.48

190 ALA

N	449 40.37	354 30.88	86 5.42
CB	464 41.72	361 31.49	57 3.59
CA	464 41.72	354 30.88	79 4.98
C	476 42.80	362 31.58	91 5.74
O	474 42.62	375 32.71	101 6.37

191 PRE

N	490 44.06	356 31.05	91 5.74
CB	504 45.31	359 31.32	125 7.88
CA	502 45.13	363 31.66	102 6.43
C	516 46.39	364 31.75	88 5.55
O	520 46.75	353 30.79	78 4.92

492 QIU

N	524	377	89
N	47.11	32.89	5.61
β	537	383	52
β	48.28	33.41	3.28
α	538	379	76
α	48.37	3.06	4.79
C	550	388	87
C	49.45	33.85	5.49
O	547	401	96
O	49.18	34.98	6.05

193 ALA

N	563	382	87
N	50.62	33.32	5.89
β	580	387	121
β	52.15	33.76	7.63
α	576	389	97
α	51.79	33.93	6.12
C	591	386	87
C	53.14	33.67	5.49
O	594	373	81
O	53.41	32.54	5.11

194 THR

N	600	398	86
N	53.95	34.72	5.42
β	613	405	57
β	55.11	35.33	3.59
α	615	396	77
α	55.29	34.54	4.86
C	625	404	94
C	56.21	35.24	5.93
O	619	414	106
O	55.66	36.11	6.69

195 PHE

N	639	401	93
N	57.45	34.98	5.87
β	648	407	132
β	58.26	35.50	8.33
α	649	409	108
α	58.35	35.68	6.81
C	666	406	103
C	59.88	35.42	6.50
O	670	392	100
O	60.24	34.19	6.31

196 DLA 674

N	418	103	
N	60.60	36.46	6.50
β	697	431	89
β	62.69	37.60	5.61
α	690	417	98
α	62.04	36.37	6.18
C	697	415	120
C	62.67	36.20	7.57
O	692	423	135
O	62.22	36.90	9.51

197 PHE

N	709	406	122
N	63.75	35.42	7.69
β	712	388	150
β	64.02	33.85	9.46
α	716	403	142
α	64.38	35.15	8.96
C	733	403	138
C	65.90	35.15	8.70
O	738	400	121
O	66.35	34.89	7.63

LEU 18

N	741	406	155
N	66.62	35.42	9.78
β	766	422	153
β	68.87	36.81	9.65
α	758	406	154
α	68.15	35.42	9.71
C	765	398	172
C	68.78	34.72	10.85
O	766	404	190
O	68.87	35.24	11.98

199 ILE

N	771	384	169
N	69.32	33.50	10.66
β	772	359	182
β	69.41	31.32	11.48
α	778	375	183
α	69.95	32.71	11.54
C	795	376	181
C	71.48	32.80	11.42
O	801	373	163
O	72.02	32.54	10.28

2017S 803			204SER 886		
N	72.20	380	198	N	79.66
β	824 74.09	398	201	β	895
α	819 73.64	381	197	α	881
C	828 74.45	372	214	C	868
O	825 74.18	373	233	O	860
		32.54	14.70		77.32
201SER 838			205 HIS 867		
N	75.34	363	206	N	77.95
β	842 75.70	337	221	β	862
α	847 76.15	353	220	α	855
C	864 77.68	353	218	C	843
O	870 78.22	348	202	O	841
		30.36	12.74		75.61
202 PRO 871			206 PRO 835		
N	78.31	359	234	N	75.07
β	891 80.11	370	253	β	818
α	888 79.84	360	234	α	824
C	892 80.20	343	234	C	811
O	904 81.28	339	226	O	805
		29.57	14.25		72.38
203 PRO 883			207 HLA 806		
N	79.39	334	245	N	72.47
β	879 79.03	313	268	β	786
α	886 79.66	318	247	α	794
C	880 79.12	308	228	C	782
O	871 78.31	314	215	O	784
		27.39	13.56		70.49
					24.08
					13.32
					205
					12.92
					209
					13.18
					219
					23.99
					13.81
					208
					13.12
					240
					15.14
					264
					16.65
					251
					15.83
					259
					16.34
					278
					17.53
					244
					15.39
					229
					14.44
					250
					15.77
					265
					16.71
					265
					16.71
					278
					17.53
					297
					18.73
					293
					18.48
					290
					18.29
					291
					18.35

208 Asp	769	286	287	212 Phe	635	335	217
N	69.14	25.82	18.10	N	57.09	29.22	13.69
CB	747 67.16	285 24.86	305 29 19.24	CB	617 55.47	346 30.18	191 12.05
CA	756 67.97	286 24.95	284 17.91	CA	622 55.92	344 30.01	214 13.50
C	747 67.16	289 25.21	264 16.65	C	609 54.76	335 29.22	224 14.13
O	743 66.80	279 24.34	251 15.83	O	605 54.40	323 28.18	215 13.56
209 Gly	743	304	261	213 Phe	603	340	241
N	66.80	26.52	16.46	N	54.22	29.66	15.20
CA	735 66.08	309 26.95	242 15.26	CB	599 53.86	329 28.70	273 17.22
C	723 65.00	321 28.00	246 15.52	CA	591 53.14	332 28.96	252 15.89
O	723 65.00	309 28.70	262 16.52	C	575 51.70	339 29.57	257 16.21
210 Ile	714	322	231	O	574 51.61	353 30.79	263 16.59
N	64.20	28.09	14.57	214 Ile	564	329	256
CB	702 63.12	346 30.18	216 13.62	N	529 50.71	335 28.70	207 16.15
CA	700 62.94	333 29.05	233 14.70	CDI	529 47.56	330 29.22	221 13.06
C	685 61.59	324 28.26	232 14.63	GGI	542 48.73	330 28.79	221 13.94
O	684 61.50	310 27.04	231 14.57	CB	538 48.37	327 28.52	244 15.39
211 Ala	673	333	233	CG2	523	334	252
N	60.51	29.05	14.70	CA	549 47.02	334 29.13	260 15.89
CB	657 59.07	318 27.74	253 15.96	C	544 49.36	327 29.13	281 16.40
CA	658 59.16	327 28.52	232 14.63	O	546 48.91	313 28.52	285 17.72
C	645 57.99	337 29.40	232 14.63	O	546 49.09	313 27.30	285 17.97
O	643 57.81	348 30.36	245 15.45				

215 SER	537	336	295
N	48.28	29.31	18.61
CB	545 49.00	332 28.96	329 20.75
C	532 47.83	331 28.87	315 19.87
C	519 46.66	341 29.75	323 20.37
O	512 46.03	349 30.44	311 19.61

216 ASN	517	341	344
N	46.48	29.75	21.70
CB	498 44.78	339 29.57	370 23.34
C	550 49.45	350 30.53	354 22.33
C	511 45.94	366 31.93	359 22.64
O	524 47.11	368 32.10	362 22.83

217 De	500	377	360
N	44.96	32.89	22.71
CB	488 43.88	399 34.80	365 23.02
C	504 45.31	393 34.28	365 23.02
C	513 46.12	392 34.19	387 24.41
O	521 46.84	403 35.15	392 24.72

218 ASP	510	379	398
N	45.85	33.06	25.10
CB	509 75.76	368 32.10	435 27.44
C	518 46.57	377 32.89	418 26.36
C	533 47.92	370 32.28	419 26.43
O	540 48.55	369 32.19	436 27.50

219 SER	538	364	401
N	48.37	31.75	25.29
CB	557 50.08	353 30.79	377 23.78
C	552 49.63	356 31.05	400 25.23
C	566 50.89	363 31.67	411 25.92
O	578 51.97	376 32.80	408 25.73

220 SER	572	353	425
N	51.43	30.79	26.80
CB	581 52.24	359 31.32	461 29.08
C	585 52.60	358 31.23	437 27.54
C	598 53.77	346 30.18	436 27.50
O	595 53.50	332 28.96	435 27.44

221 De	611	351	437
N	54.94	30.62	27.56
CB	639 57.45	350 30.53	438 27.62
C	624 56.10	341 29.75	436 27.50
C	625 56.19	331 28.87	455 28.70
O	626 56.28	336 29.31	473 29.83

222 PRO	626	316	451
N	56.28	27.56	28.44
CB	623 56.01	290 25.30	459 28.95
C	627 56.37	305 26.61	469 29.58
C	643 57.81	304 26.52	478 30.15
O	653 58.71	313 27.30	473 29.83

	223 SEP	645	293	493	227 GLY	735	289	395
29	N	57.99	25.56	31.09	N	66.08	25.21	24.91
	β	657	288	527	α	740	276	383
8	α	59.07	25.12	33.24	α	66.53	24.08	24.16
3	α	659	291	503	α	732	272	363
	α	59.25	25.38	31.72	α	65.81	23.73	22.89
	α	671	283	490	α	729	282	350
2	α	60.33	24.69	30.90	α	65.54	24.60	22.07
	α	670	270	482	α	729	257	360
73	α	60.24	23.55	30.40	228 PRG	729	257	360
	224 GLY	683	292	487	N	65.54	22.42	22.71
80	N	61.41	25.47	30.72	β	724	234	343
	α	696	286	475	α	65.09	20.41	21.63
8	α	62.58	24.95	29.96	α	722	252	340
	α	690	285	452	α	64.92	21.98	21.44
56	α	62.04	24.86	28.51	α	705	254	344
	α	694	274	441	α	63.39	22.16	21.70
0	α	62.40	23.90	27.81	α	696	253	329
	225 SEP	682	296	445	α	62.58	22.07	20.75
4	N	61.32	25.82	28.07	229 Leu	701	258	363
	β	665	309	424	N	63.03	22.51	22.89
6	α	59.79	26.95	26.74	β	684	261	393
	α	676	297	424	α	61.50	22.77	24.79
2	α	69.78	25.91	26.74	α	686	261	369
	α	691	298	412	α	61.68	22.77	23.27
0	α	62.13	25.99	25.98	α	680	276	358
	α	692	297	393	α	61.14	24.08	22.58
0	α	62.22	25.91	24.79	α	668	281	362
	226 SEP	702	301	425	α	60.06	24.57	22.83
83	N	63.12	26.26	26.80	230 Leu	689	282	344
	β	731	306	430	N	61.95	24.60	21.70
4	α	65.72	26.69	27.12	β	679	292	311
	α	717	303	416	α	61.05	25.47	19.61
5	α	64.47	26.43	26.24	α	685	296	333
	α	722	289	405	α	61.59	25.82	21.00
8	α	64.92	25.21	25.54	α	673	306	342
	α	714	277	406	α	60.51	26.69	21.57
5	α	64.20	24.16	25.61	α	666	315	331
					α	59.88	27.48	20.88

231 QLY 671	304	363
N 60.33	26.52	22.89
α 659 59.25	313 27.30	374 23.59
C 644 57.90	312 27.22	363 22.89
O 635 57.09	323 28.18	363 22.89

232 LRU 641	299	355
N 57.63	26.08	22.39
CB 627 56.37	293 25.56	320 20.18
α 626 56.28	296 25.82	344 21.70
C 619 55.65	283 24.69	357 22.52
O 606 54.49	283 24.69	361 22.77

233 Phe 628	272	363
N 56.46	23.73	22.89
CB 624 56.10	245 21.37	360 22.71
α 623 56.01	259 22.59	375 23.65
C 630 56.64	255 22.24	396 24.98
O 643 57.81	255 22.24	399 25.16

234 PRO 620	252	412
N 55.74	21.98	25.98
CB 612 55.02	249 21.72	447 28.19
α 626 56.28	248 21.63	433 27.31
C 633 56.91	233 20.32	431 27.18
O 635 57.09	227 19.80	413 26.05

235 ASP 636	226	449
N 57.18	19.71	28.32
CB 652 58.62	211 18.41	471 29.71
α 643 57.81	211 18.41	449 28.32
C 630 56.64	200 17.45	449 28.32
O 623 56.01	197 17.18	465 29.33

236 PLA 627	193	430
N 56.37	16.84	27.12
CB 599 53.86	190 16.57	429 27.06
α 615 55.29	183 15.96	428 26.99
C 617 55.47	176 15.35	406 25.61
O 617 55.47	185 16.14	390 24.60

237 BSN 618	161	405
N 55.56	14.04	25.54
CB 636 57.18	159 13.87	377 23.78
α 621 55.83	154 13.43	384 24.22
C 622 55.92	136 11.86	385 24.28
O 610 54.85	128 11.17	385 24.28
O2 635 57.09	131 11.43	385 24.28

10th

Circuit →

⊗ Certification →

Binding →

Submissi 2

KRIE 1, (ASB)